

# Motion planing and tracking for differentially flat systems

Pierre Rouchon  
Mines-ParisTech,  
Centre Automatique et Systèmes  
Mathématiques et Systèmes  
`pierre.rouchon@mines-paristech.fr`

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# Outline

## Introduction

## Two ODE examples

- Pendulum systems

- Nonholonomic car with trailers

## ODE: several definitions of flat-systems

- An elementary definition based on inversion

- The intrinsic definition with  $D$ -variety (diffiety)

- An extrinsic definition

- A time dependent definition

## PDE: two kind of flat examples

- Wave and delays

- Diffusion and Gevrey functions

## Conclusion for PDE

## Conclusion for ODE: flatness characterization is an open problem

- Systems with only one control

- Driftless systems as Pfaffian system

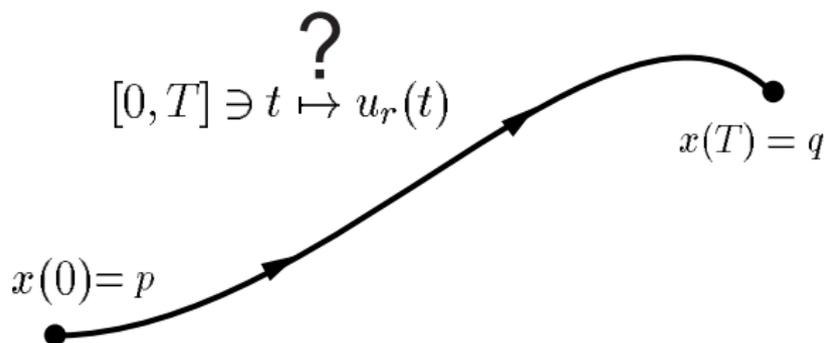
- Ruled manifold criterion

- Symmetry preserving flat-output

## Interest of flat systems

1. History: "integrability" for under-determined systems of differential equations (Monge, Hilbert, Cartan, ....).
2. Control theory: flat systems admit simple solutions to the motion planning and tracking problems (Fliess and coworkers 1991 and later).
3. Books on differentially flat systems:
  - ▶ H. Sira-Ramirez and S.K. Agarwal: Differentially flat systems. CRC, 2004.
  - ▶ J. Lévine: Analysis and Control of Nonlinear Systems : A Flatness-Based Approach. Springer-Verlag, 2009.
  - ▶ J. Rudolph: Flatness Based Control of Distributed Parameter Systems. Shaker, Germany. 2003.

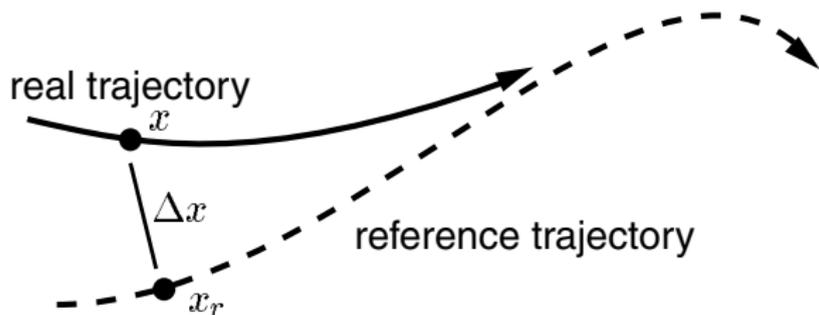
## Motion planning: controllability.



Difficult problem due to integration of

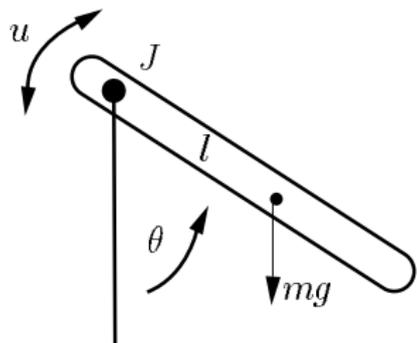
$$\frac{d}{dt}x = f(x, u_r(t)), \quad x(0) = p.$$

Tracking for  $\frac{d}{dt}x = f(x, u)$ : stabilization.



Compute  $\Delta u$ ,  $u = u_r + \Delta u$ , depending  $\Delta x$  (feedback), such that  $\Delta x = x - x_r$  tends to 0 (stabilization).

## The simplest robot



- ▶ Newton ODE):

$$\frac{d^2}{dt^2}\theta = -p \sin(\theta) + u$$

Non linear oscillator with scalar input  $u$  and parameter  $p > 0$ .

- ▶ **Computed torque method:**  
 $u_r = \frac{d^2}{dt^2}\theta_r + p \sin \theta_r$  provides an explicit parameterization via  $KC^2$  function:  $t \mapsto \theta_r(t)$ , the **flat output**.

**Motion planing and tracking** ( $\xi, \omega_0 > 0$ , two **feedback** gains)

$$u \left( t, \theta, \frac{d}{dt}\theta \right) = \frac{d^2}{dt^2}\theta_r + p \sin \theta - 2\xi\omega_0 \left( \frac{d}{dt}\theta - \frac{d}{dt}\theta_r \right) - (\omega_0)^2 \sin(\theta - \theta_r)$$

where  $t \mapsto \theta_r(t)$  defines the **reference trajectory** (control goal).

## Fully actuated mechanical systems

The computed torque method for

$$\frac{d}{dt} \left[ \frac{\partial L}{\partial \dot{q}} \right] = \frac{\partial L}{\partial q} + M(q)u$$

consists in setting  $t \mapsto q(t)$  to obtain  $u$  as a function of  $q$ ,  $\dot{q}$  and  $\ddot{q}$ .

(Fully actuated:  $\dim q = \dim u$  and  $M(q)$  invertible).

## Oscillators and linear systems

System with 2 ODEs and 3 unknowns  $(x_1, x_2, u)$  ( $a_1, a_2 > 0$  and  $a_1 \neq a_2$ )

$$\frac{d^2}{dt^2} x_1 = -a_1(x_1 - u), \quad \frac{d^2}{dt^2} x_2 = -a_2(x_2 - u)$$

defines a free module<sup>1</sup> with basis  $y = \frac{a_2 x_1 - a_1 x_2}{a_2 - a_1}$ :

$$\begin{cases} x_1 = y + \frac{d^2}{dt^2} y / a_2, & \frac{d}{dt} x_1 = \frac{d}{dt} y + \frac{d^3 y}{dt^3} / a_2 \\ x_2 = y + \frac{d^2}{dt^2} y / a_1, & \frac{d}{dt} x_2 = \frac{d}{dt} y + \frac{d^3 y}{dt^3} / a_1 \\ u = y + \left( \frac{1}{a_1} + \frac{1}{a_2} \right) \frac{d^2}{dt^2} y + \left( \frac{1}{a_1 a_2} \right) \frac{d^4}{dt^4} y \end{cases}$$

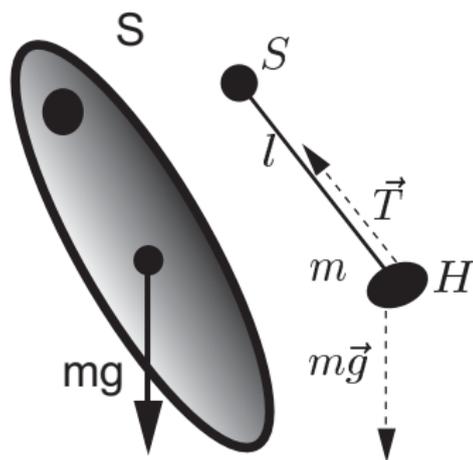
Reference trajectory for equilibrium  $x_1 = x_2 = u = 0$  at  $t = 0$  to equilibrium  $x_1 = x_2 = u = D$  at  $t = T > 0$ :

$$y(t) = \begin{cases} 0 & \text{si } t \leq 0, \\ \frac{(t)^4}{t^4 + (T-t)^4} D & \text{si } t \in [0, T], \\ D & \text{si } t \geq T. \end{cases}$$

Generalization to  $n$  oscillators and any linear controllable system,  $\frac{d}{dt} X = AX + Bu$ .

<sup>1</sup>See the work of Alban Quadrat and co-workers.... 

## $2k\pi$ juggling robot: prototype of implicit flat system



Isochronous punctual pendulum  $H$   
(Huygens) :

$$m \frac{d^2}{dt^2} H = \vec{T} + m\vec{g}$$

$$\vec{T} // \vec{HS}$$

$$\|\vec{HS}\|^2 = l$$

- ▶ The suspension point  $S \in \mathbb{R}^3$  stands for the control input
- ▶ The **oscillation center**  $H \in \mathbb{R}^3$  is the flat output: since  $\vec{T}/m = \frac{d^2}{dt^2} H - \vec{g}$  et  $\vec{T} // \vec{HS}$ ,  $S$  is solution of the algebraic system:

$$\vec{HS} // \frac{d^2}{dt^2} H - \vec{g} \quad \text{and} \quad \|\vec{HS}\|^2 = l.$$

## Return of the pendulum and smooth branch switch

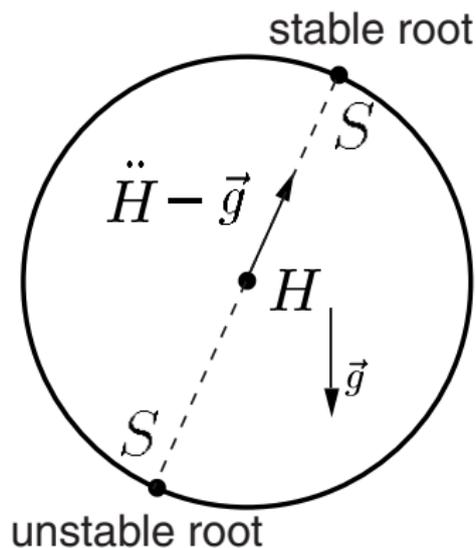
In a vertical plane:  $H$  of coordinates  $(y_1, y_2)$  and  $S$  of coordinates  $(u_1, u_2)$  satisfy

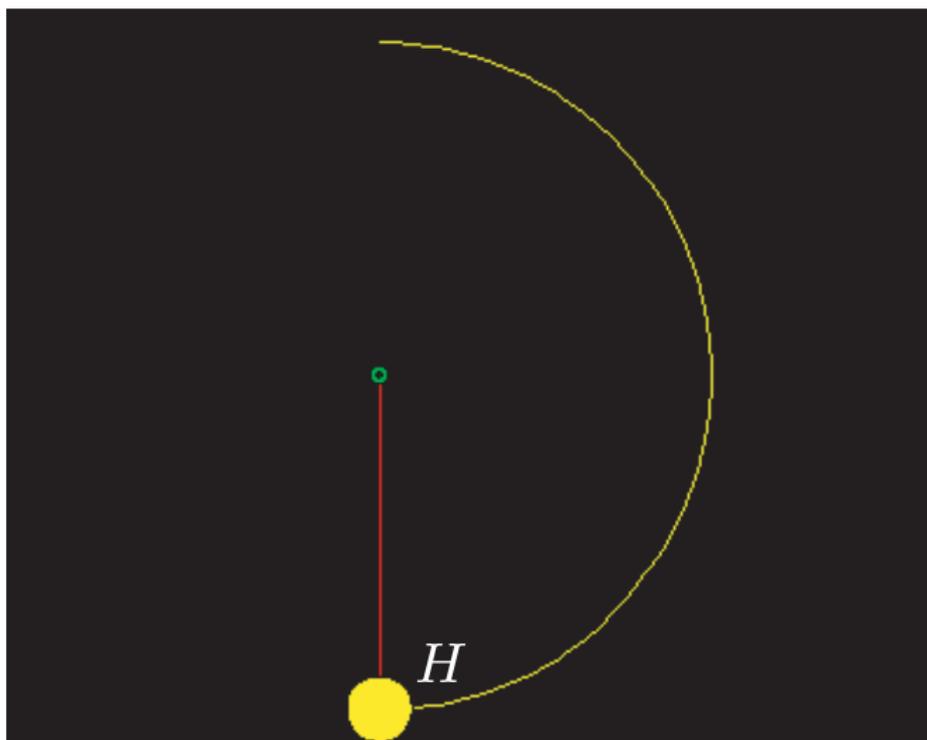
$$(y_1 - u_1)^2 + (y_2 - u_2)^2 = l, \quad (y_1 - u_1) \left( \frac{d^2}{dt^2} y_2 + g \right) = (y_2 - u_2) \frac{d^2}{dt^2} y_1.$$

Find  $[0, T] \ni t \mapsto y(t) \in C^2$  such that  $y(0) = (0, -l)$ ,  $y(T) = (0, l)$  and  $y^{(1,2)}(0, T) = 0$ , and such that exists also  $[0, T] \ni t \mapsto u(t) \in C^0$  with  $u(0) = u(T) = 0$  (switch between the stable and the unstable branches).

## Planning the inversion trajectory

Any smooth trajectory connecting the stable to the unstable equilibrium is such that  $\ddot{H}(t) = \vec{g}$  for at least one time  $t$ . During the motion there is a switch from the stable root to the unstable root (singularity crossing when  $\ddot{H} = \vec{g}$ )



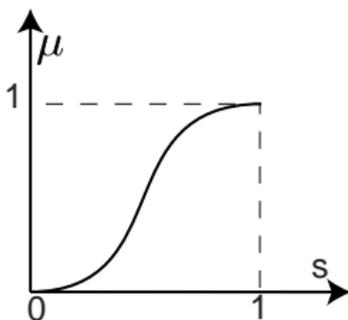


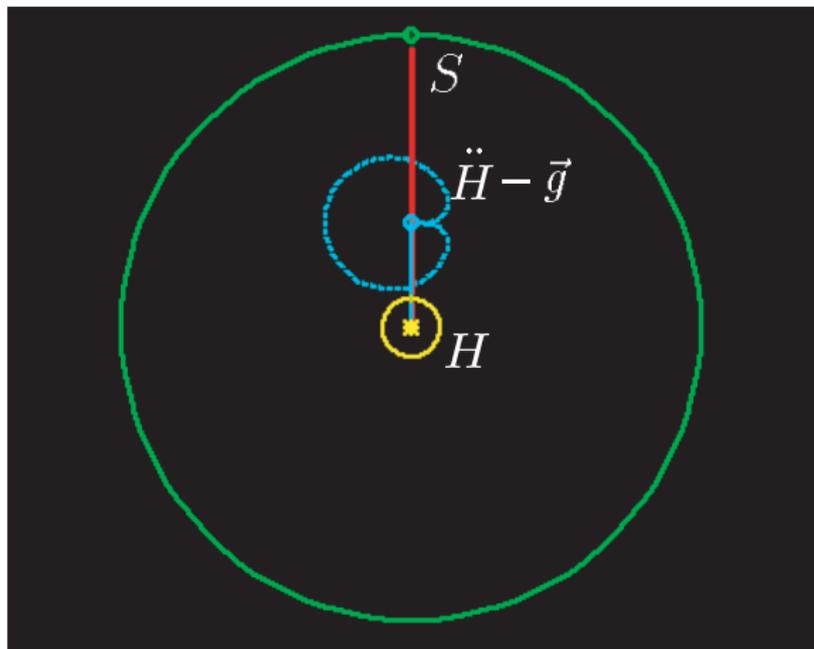
## Crossing smoothly the singularity $\ddot{H} = \vec{g}$

The geometric path followed by  $H$  is a half-circle of radius  $l$  of center  $O$ :

$$H(t) = O + l \begin{bmatrix} \sin \theta(s) \\ -\cos \theta(s) \end{bmatrix} \text{ with } \theta(s) = \mu(s)\pi, \quad s = t/T \in [0, 1]$$

where  $T$  is the transition time and  $\mu(s)$  a sigmoid function of the form:





## Time scaling and dilatation of $\ddot{H} - \vec{g}$

Denote by  $'$  derivation with respect to  $s$ . From

$$H(t) = 0 + I \begin{bmatrix} \sin \theta(s) \\ -\cos \theta(s) \end{bmatrix}, \quad \theta(s) = \mu(t/T)\pi$$

we have

$$\ddot{H} = H''/T^2.$$

Changing  $T$  to  $\alpha T$  yields to a dilation of factor  $1/\alpha^2$  of the closed geometric path described by  $\ddot{H} - \vec{g}$  for  $t \in [0, T]$  ( $\ddot{H}(0) = \ddot{H}(T) = 0$ ), the dilation center being  $-\vec{g}$ .

The inversion time is obtained when this closed path passes through 0. This construction holds true for generic  $\mu$ .

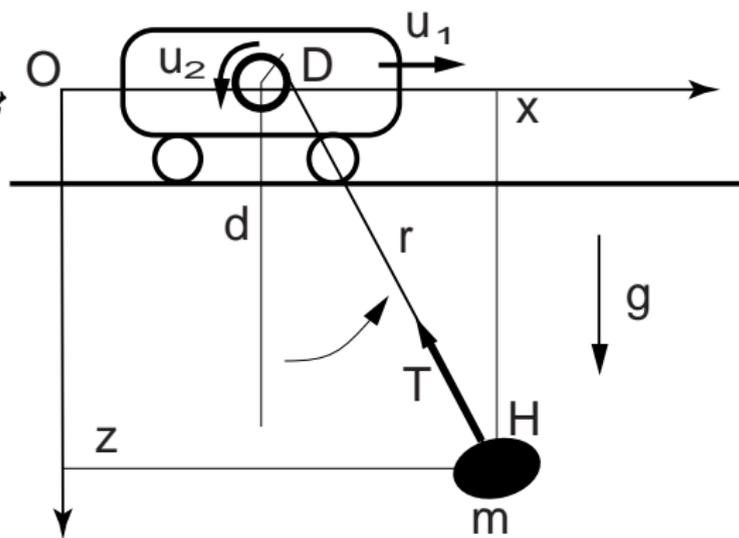
## The crane

$$m\ddot{H} = \vec{T} + m\vec{g}$$

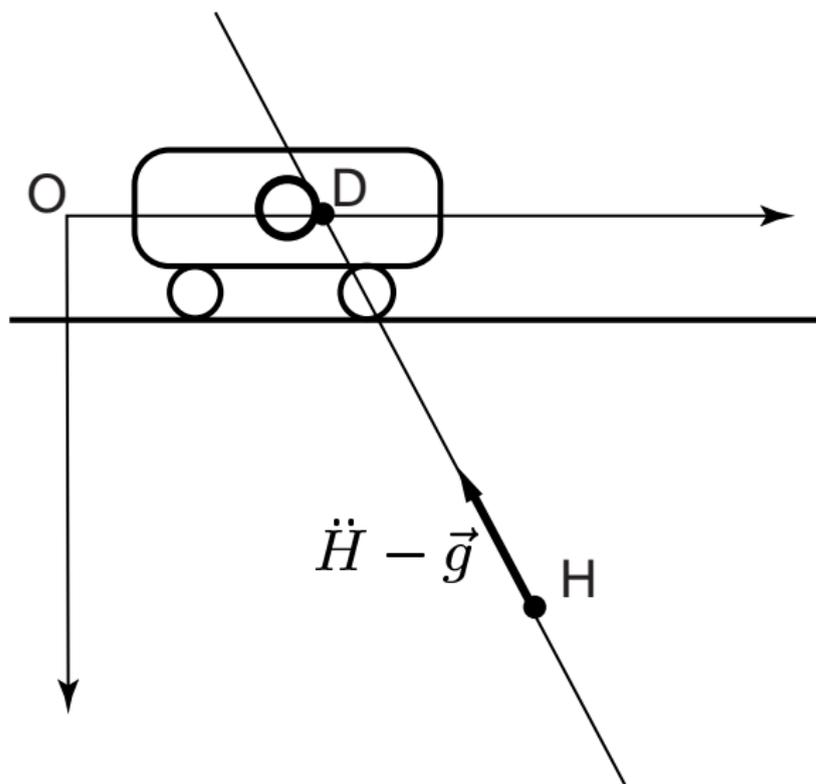
$$\vec{T} // \overrightarrow{HD}$$

$$HD = r$$

$$\overrightarrow{OD} \cdot \vec{k} = 0$$

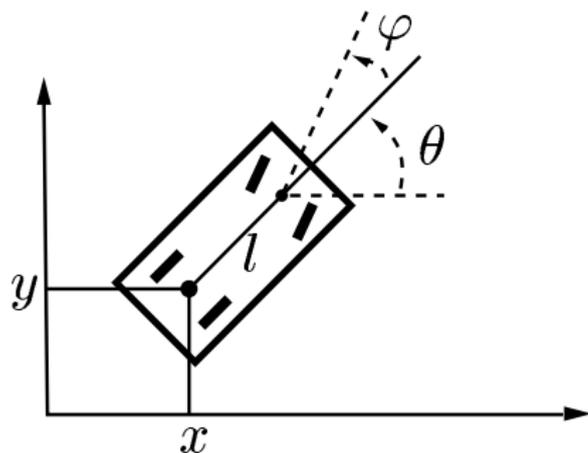


## The geometric construction for the crane

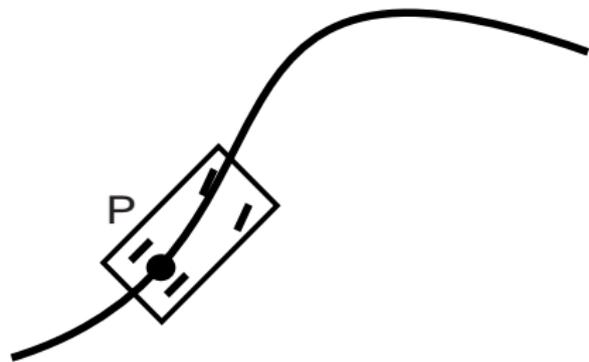


Singularity when  $\ddot{H} - \vec{g}$  is horizontal.

## Single car <sup>2</sup>



$$\begin{cases} \frac{d}{dt}x = v \cos \theta \\ \frac{d}{dt}y = v \sin \theta \\ \frac{d}{dt}\theta = \frac{v}{l} \tan \varphi = \omega \end{cases}$$



$$\begin{cases} v = \pm \left\| \frac{d}{dt}P \right\| \\ \begin{bmatrix} \cos \theta \\ \sin \theta \end{bmatrix} = \frac{\frac{d}{dt}P}{v} \\ \tan \varphi = \frac{l \det(\ddot{P}, \dot{P})}{v \sqrt{|v|}} \end{cases}$$

<sup>2</sup>For modeling and control of non-holonomic systems, see, e.g., B.

## The time scaling symmetry

For any  $T \mapsto \sigma(T)$ , the transformation

$$t = \sigma(T), \quad (x, y, \theta) = (X, Y, \Theta), \quad (v, \omega) = (V, \Omega)/\sigma'(t)$$

leave the equations

$$\frac{d}{dt}x = v \cos \theta, \quad \frac{d}{dt}y = v \sin \theta, \quad \frac{d}{dt}\theta = \omega$$

unchanged:

$$\frac{d}{dT}X = V \cos \Theta, \quad \frac{d}{dT}Y = V \sin \Theta, \quad \frac{d}{dT}\Theta = \Omega.$$

## SE(2) invariance

For any  $(a, b, \alpha)$ , the transformation

$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} X \cos \alpha - Y \sin \alpha + a \\ X \sin \alpha + Y \cos \alpha + b \end{bmatrix}, \quad \theta = \Theta - \alpha, \quad (v, \omega) = (V, \Omega)$$

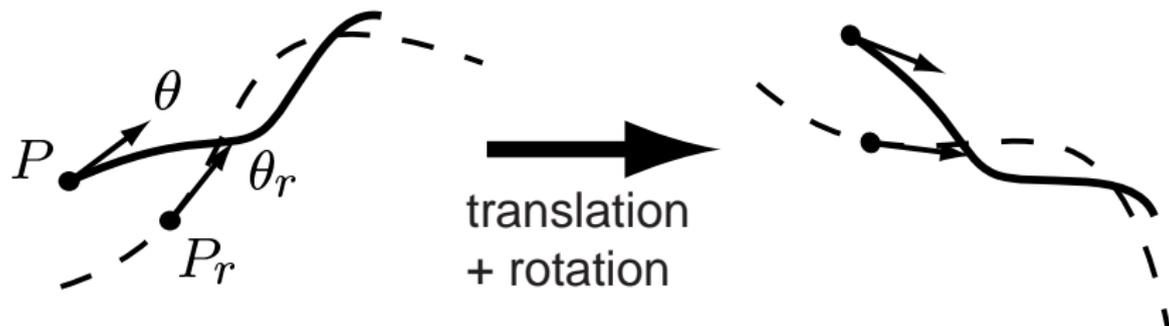
leave the equations

$$\frac{d}{dt}x = v \cos \theta, \quad \frac{d}{dt}y = v \sin \theta, \quad \frac{d}{dt}\theta = \omega$$

unchanged:

$$\frac{d}{dt}X = V \cos \Theta, \quad \frac{d}{dt}Y = V \sin \Theta, \quad \frac{d}{dt}\Theta = \Omega.$$

## Invariant tracking<sup>3</sup>



<sup>3</sup>For a general setting see: Ph. Martin, P. R., J. Rudolph: Invariant tracking, ESAIM: Control, Optimisation and Calculus of Variations, 10:1–13,2004.

## Invariant tracking for the car: goal

Given the reference trajectory

$$t \mapsto \mathbf{s}_r \mapsto P_r(\mathbf{s}_r), \quad \theta_r(\mathbf{s}_r), \quad \mathbf{v}_r = \dot{\mathbf{s}}_r, \quad \omega_r = \dot{\mathbf{s}}_r \kappa_r(\mathbf{s}_r)$$

and the state  $(P, \theta)$

Find an invariant controller

$$\mathbf{v} = \mathbf{v}_r + \dots, \quad \omega = \omega_r + \dots$$

## Invariant tracking for the car: time-scaling

Set

$$v = \bar{v} \dot{s}_r, \quad \omega = \bar{\omega} \dot{s}_r$$

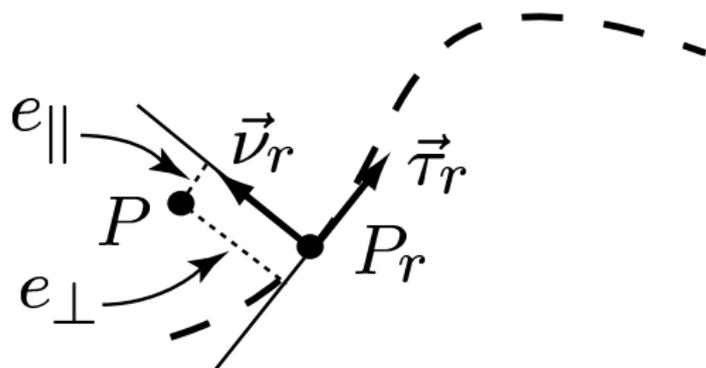
and denote by  $'$  derivation versus  $s_r$ .

Equations remain unchanged

$$P' = \bar{v} \vec{\tau}, \quad \vec{\tau}' = \bar{\omega} \vec{\nu}$$

with  $P = (x, y)$ ,  $\vec{\tau} = (\cos \theta, \sin \theta)$  and  $\vec{\nu} = (-\sin \theta, \cos \theta)$ .

## Invariant errors



Construct the decoupling and/or linearizing controller with the two following invariant errors

$$e_{\parallel} = (P - P_r) \cdot \vec{\tau}_r, \quad e_{\perp} = (P - P_r) \cdot \vec{v}_r.$$

## Computations of $e_{\parallel}$ and $e_{\perp}$ derivatives

Since  $e_{\parallel} = (P - P_r) \cdot \vec{\tau}_r$  and  $e_{\perp} = (P - P_r) \cdot \vec{\nu}_r$  we have (remember that  $' = d/ds_r$ )

$$e'_{\parallel} = (P' - P'_r) \cdot \vec{\tau}_r + (P - P_r) \cdot \vec{\tau}'_r.$$

But  $P' = \bar{\nu} \vec{\tau}$ ,  $P'_r = \vec{\tau}_r$  and  $\vec{\tau}'_r = \kappa_r \vec{\nu}_r$ , thus

$$e'_{\parallel} = \bar{\nu} \vec{\tau} \cdot \vec{\tau}_r - 1 + \kappa_r (P - P_r) \cdot \vec{\nu}_r.$$

Similar computations for  $e'_{\perp}$  yield:

$$e'_{\parallel} = \bar{\nu} \cos(\theta - \theta_r) - 1 + \kappa_r e_{\perp}, \quad e'_{\perp} = \bar{\nu} \sin(\theta - \theta_r) - \kappa_r e_{\parallel}.$$

## Computations of $\mathbf{e}_{\parallel}$ and $\mathbf{e}_{\perp}$ second derivatives

Derivation of

$$\mathbf{e}'_{\parallel} = \bar{v} \cos(\theta - \theta_r) - 1 + \kappa_r \mathbf{e}_{\perp}, \quad \mathbf{e}'_{\perp} = \bar{v} \sin(\theta - \theta_r) - \kappa_r \mathbf{e}_{\parallel}$$

with respect to  $s_r$  gives

$$\begin{aligned} \mathbf{e}''_{\parallel} &= \bar{v}' \cos(\theta - \theta_r) - \bar{\omega} \bar{v} \sin(\theta - \theta_r) \\ &\quad + 2\kappa_r \bar{v} \sin(\theta - \theta_r) + \kappa'_r \mathbf{e}_{\perp} - \kappa_r^2 \mathbf{e}_{\parallel} \end{aligned}$$

$$\begin{aligned} \mathbf{e}''_{\perp} &= \bar{v}' \sin(\theta - \theta_r) + \bar{\omega} \bar{v} \cos(\theta - \theta_r) \\ &\quad - 2\kappa_r \bar{v} \cos(\theta - \theta_r) - \kappa'_r \mathbf{e}_{\parallel} + \kappa_r + \kappa_r^2 \mathbf{e}_{\parallel}. \end{aligned}$$

## The dynamics feedback in $s_r$ time-scale

We have obtain

$$\begin{aligned} e''_{\parallel} &= \bar{v}' \cos(\theta - \theta_r) - \bar{\omega} \bar{v} \sin(\theta - \theta_r) \\ &\quad + 2\kappa_r \bar{v} \sin(\theta - \theta_r) + \kappa'_r e_{\perp} - \kappa_r^2 e_{\parallel} \end{aligned}$$

$$\begin{aligned} e''_{\perp} &= \bar{v}' \sin(\theta - \theta_r) + \bar{\omega} \bar{v} \cos(\theta - \theta_r) \\ &\quad - 2\kappa_r \bar{v} \cos(\theta - \theta_r) - \kappa'_r e_{\parallel} + \kappa_r + \kappa_r^2 e_{\parallel}. \end{aligned}$$

Choose  $\bar{v}'$  and  $\bar{\omega}$  such that

$$\begin{aligned} e''_{\parallel} &= - \left( \frac{1}{L_{\parallel}^1} + \frac{1}{L_{\parallel}^2} \right) e'_{\parallel} - \left( \frac{1}{L_{\parallel}^1 L_{\parallel}^2} \right) e_{\parallel} \\ e''_{\perp} &= - \left( \frac{1}{L_{\perp}^1} + \frac{1}{L_{\perp}^2} \right) e'_{\perp} - \left( \frac{1}{L_{\perp}^1 L_{\perp}^2} \right) e_{\perp} \end{aligned}$$

Possible around a large domain around the reference trajectory since the determinant of the decoupling matrix is  $\bar{v} \approx 1$ .

## The dynamics feedback in physical time-scale

In the  $s_r$  scale, we have the following dynamic feedback

$$\bar{v}' = \Phi(\bar{v}, P, P_r, \theta, \theta_r, \kappa_r, \kappa_r')$$

$$\bar{\omega} = \Psi(\bar{v}, P, P_r, \theta, \theta_r, \kappa_r, \kappa_r')$$

Since  $' = d/ds_r = d/(\dot{s}_r dt)$  we have

$$\frac{d\bar{v}}{dt} = \Phi(\bar{v}, P, P_r, \theta, \theta_r, \kappa_r, \kappa_r') \dot{s}_r(t)$$

$$\bar{\omega} = \Psi(\bar{v}, P, P_r, \theta, \theta_r, \kappa_r, \kappa_r')$$

and the real control is

$$v = \bar{v} \dot{s}_r(t), \quad \tan \phi = \frac{l\bar{\omega}}{\bar{v}}$$

Nothing blows up when  $\dot{s}_r(t)$  tends to 0: the controller is well defined around steady-state via a simple use of time-scaling symmetry

## Conversion into chained form destroys $SE(2)$ invariance

The car model

$$\frac{d}{dt}x = v \cos \theta, \quad \frac{d}{dt}y = v \sin \theta, \quad \frac{d}{dt}\theta = \frac{v}{l} \tan \varphi$$

can be transformed into chained form

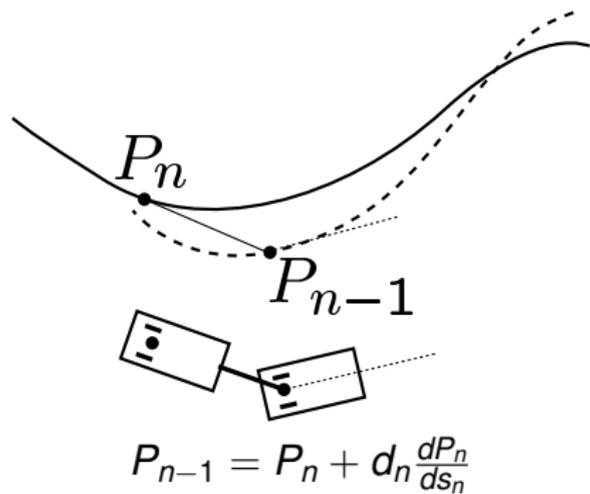
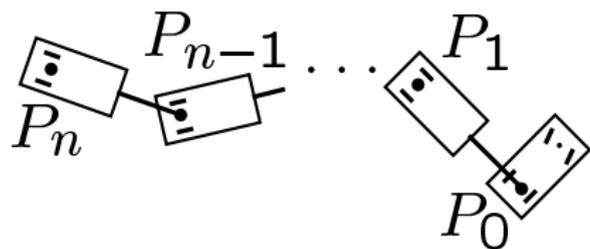
$$\frac{d}{dt}x_1 = u_1, \quad \frac{d}{dt}x_2 = u_2, \quad \frac{d}{dt}x_3 = x_2 u_1$$

via change of coordinates and static feedback

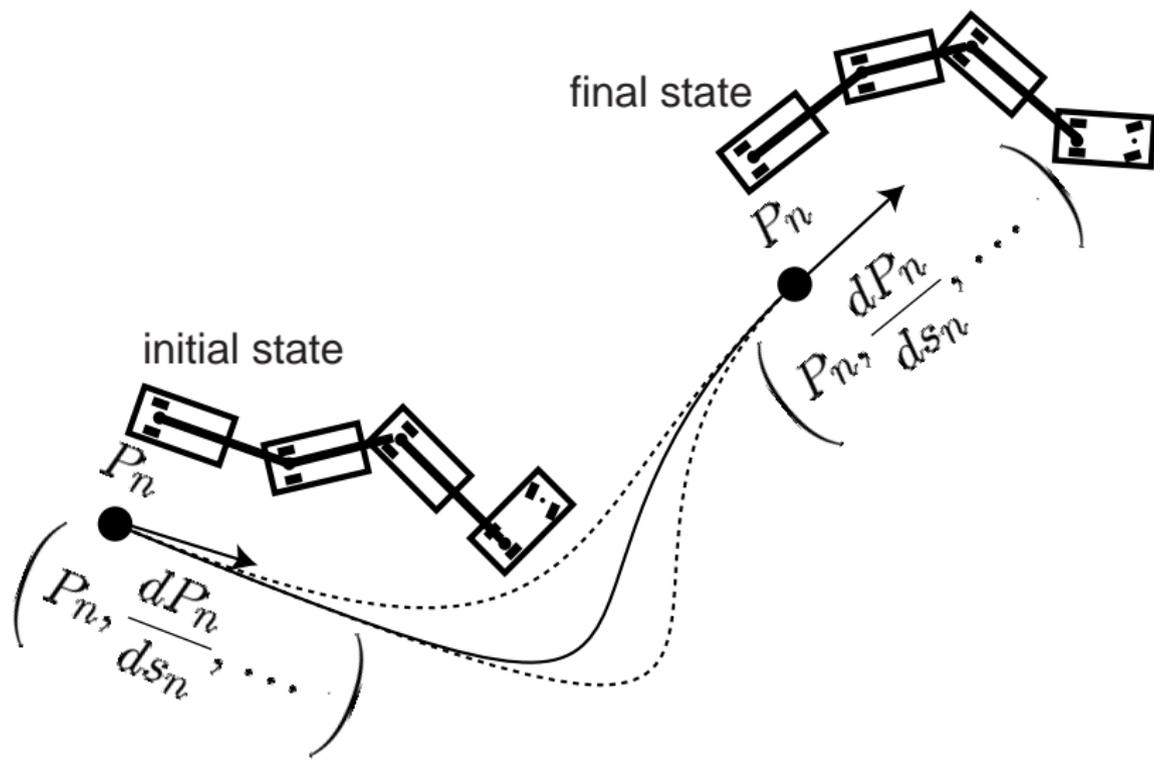
$$x_1 = x, \quad x_2 = \frac{dy}{dx} = \tan \theta, \quad x_3 = y.$$

But the symmetries are not preserved in such coordinates: one privileges axis  $x$  versus axis  $y$  without any good reason. The behavior of the system seems to depend on the origin you take to measure the angle (artificial singularity when  $\theta = \pm\pi/2$ ).

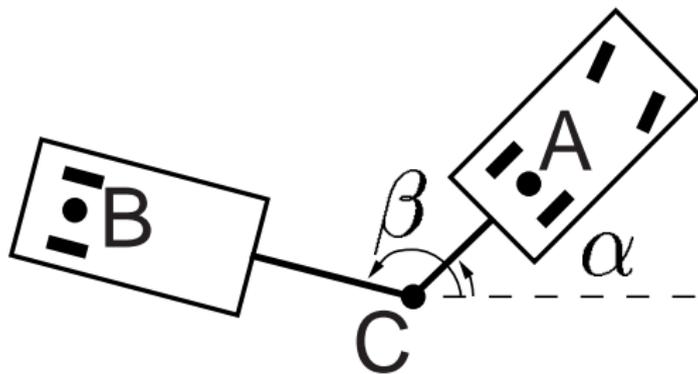
## The standard $n$ -trailers system



## Motion planning for the standard $n$ trailers system



## The general 1-trailer system (CDC93)



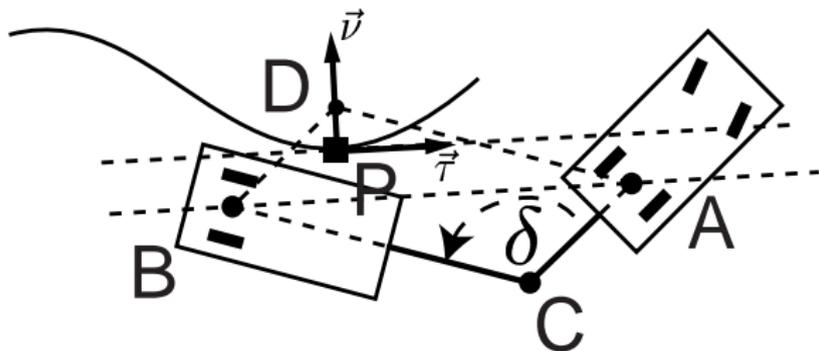
Rolling without slipping conditions ( $A = (x, y)$ ,  $u = (v, \varphi)$ ):

$$\frac{d}{dt}x = v \cos \alpha$$

$$\frac{d}{dt}y = v \sin \alpha$$

$$\frac{d}{dt}\alpha = \frac{v}{l} \tan \varphi$$

$$\frac{d}{dt}\beta = \frac{v}{b} \left( \frac{a}{l} \tan \varphi \cos(\beta - \alpha) + \sin(\beta - \alpha) \right).$$



With  $\delta = \widehat{BCA}$  we have

$$D = P - L(\delta)\vec{v} \quad \text{with} \quad L(\delta) = ab \int_0^{\pi+\delta} \frac{-\cos \sigma}{\sqrt{a^2 + b^2 + 2ab \cos \sigma}} d\sigma$$

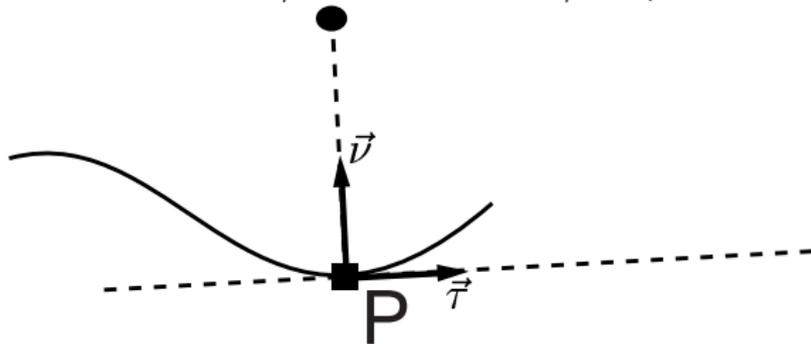
Curvature is given by

$$K(\delta) = \frac{\sin \delta}{\cos \delta \sqrt{a^2 + b^2 - 2ab \cos \delta} - L(\delta) \sin \delta}$$

## The geometric construction

Assume that  $s \mapsto P(s)$  is known. Let us show how to deduce  $(A, B, \alpha, \beta)$  the system configuration.

We know thus  $P$ ,  $\vec{\tau} = dP/ds$  and  $\kappa = d\theta/ds$  ( $\theta$  is the angle of  $\vec{\tau}$ ):

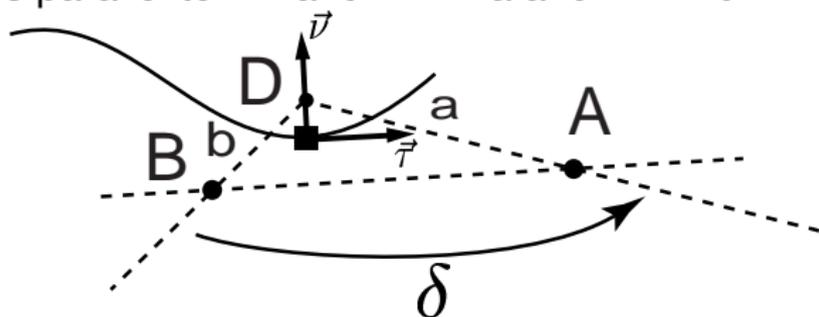


## The geometric construction

From  $\kappa$  we deduce  $\delta = \widehat{BCA} = \widehat{BDA}$  by inverting  $\kappa = K(\delta)$ .

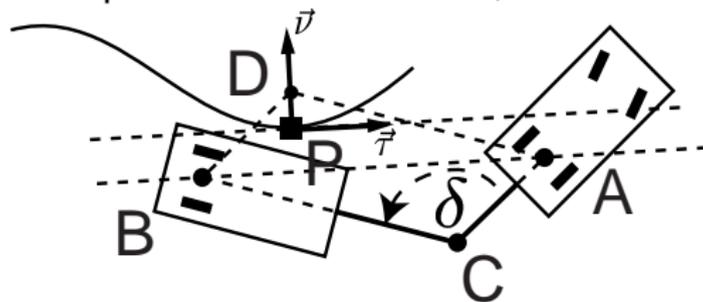
$D$  is then known since  $D = P - L(\delta)\vec{v}$ .

Finally  $\vec{\tau}$  is parallel to  $AB$  and  $DB = a$  and  $DA = b$ .



## The complete construction

One to one correspondence between  $P$ ,  $\vec{\tau}$  and  $\kappa$  and  $(A, \alpha, \beta)$ .



## Differential forms

Eliminate  $v$  from

$$\frac{d}{dt}x = v \cos \alpha, \quad \frac{d}{dt}y = v \sin \alpha, \quad \frac{d}{dt}\alpha = \frac{v}{l} \tan \varphi, \quad \frac{d}{dt}\beta = \dots$$

to have 3 equations with 5 variables

$$\sin \alpha \frac{d}{dt}x - \cos \alpha \frac{d}{dt}y = 0$$

$$\frac{d}{dt}\alpha - \left( \frac{\tan \varphi \cos \alpha}{l} \right) \frac{d}{dt}x - \left( \frac{\tan \varphi \sin \alpha}{l} \right) \frac{d}{dt}y = 0$$

$$\frac{d}{dt}\beta \dots$$

defining a module of differential forms,  $l = \{\eta_1, \eta_2, \eta_3\}$

$$\eta_1 = \sin \alpha \, dx - \cos \alpha \, dy$$

$$\eta_2 = d\alpha - \left( \frac{\tan \varphi \cos \alpha}{l} \right) dx - \left( \frac{\tan \varphi \sin \alpha}{l} \right) dy$$

$$\eta_3 = d\beta - \dots$$

Following <sup>4</sup>, compute the sequence  $I = I^{(0)} \supseteq I^{(1)} \supseteq I^{(2)} \dots$   
where

$$I^{(k+1)} = \{\eta \in I^{(k)} \mid d\eta = 0 \pmod{I^{(k)}}\}$$

and find that

$$\dim I^{(0)} = 3, \quad \dim I^{(1)} = 2, \quad \dim I^{(2)} = 1, \quad \dim I^{(3)} = 0.$$

The Cartesian coordinates  $(X, Y)$  of  $P$  are obtained via the Pfaff normal form of the differential form  $\mu$  generating  $I^{(2)}$

$$\mu = f(\alpha, \beta) dX + g(\alpha, \beta) dY.$$

$(X, Y)$  is not unique;  $SE(2)$  invariance simplifies computations.

---

<sup>4</sup>E. Cartan: Sur l'intégration de certains systèmes indéterminés d'équations différentielles. J. für reine und angew. Math. Vol. 145, 1915.

## Contact systems:

The driftless system  $\frac{d}{dt}x = f_1(x)u_1 + f_2(x)u_2$  is also a Pfaffian system of codimension 2

$$\omega_i \equiv \sum_{j=1}^n a_i^j(x) dx_j = 0, \quad i = 1, \dots, n-2.$$

Pfaffian systems equivalent via changes of  $x$ -coordinates to contact systems (related to chained-form, Murray-Sastry 1993)

$$dx_2 - x_3 dx_1 = 0, \quad dx_3 - x_4 dx_1 = 0, \quad \dots \quad dx_{n-1} - x_n dx_1 = 0$$

are mainly characterized by the derived flag (Weber(1898), Cartan(1916), Goursat (1923), Giaro-Kumpera-Ruiz(1978), Murray (1994), Pasillas-Respondek (2000), ...).

## Interest of contact systems (chained form):

$$dx_2 - x_3 dx_1 = 0, \quad dx_3 - x_4 dx_1 = 0, \quad \dots \quad dx_{n-1} - x_n dx_1 = 0$$

The general solution reads in terms of  $z \mapsto w(z)$  and its derivatives,

$$x_1 = z, \quad x_2 = w(z), \quad x_3 = \frac{dw}{dz}, \quad \dots, \quad x_n = \frac{d^{n-2}w}{dz^{n-2}}.$$

In this case, the general solution of  $\frac{d}{dt}x = f_1(x)u_1 + f_2(x)u_2$  reads in terms of  $t \mapsto z(t)$  any  $C^1$  time function and any  $C^{n-2}$  function of  $z$ ,  $z \mapsto w(z)$ . The quantities  $x_1 = z(t)$  and  $x_2 = w(z(t))$  play here a special role. We call them the flat output.

## An elementary definition based on inversion

- ▶ **Explicit control systems:**  $\frac{d}{dt}x = f(x, u)$  ( $x \in \mathbb{R}^n$ ,  $u \in \mathbb{R}^m$ ) is flat, iff, exist  $\alpha \in \mathbb{N}$  and  $h(x, u, \dots, u^{(\alpha)}) \in \mathbb{R}^m$  such that the **generic** solution of

$$\frac{d}{dt}x = f(x, u), \quad y = h(x, u, \dots, u^{(\alpha)})$$

reads ( $\beta \in \mathbb{N}$ )

$$x = \mathcal{A}(y, \dots, y^{(\beta)}), \quad u = \mathcal{B}(y, \dots, y^{(\beta+1)})$$

- ▶ **Under-determined systems:**  $F(x, \dots, x^{(r)}) = 0$  ( $x \in \mathbb{R}^n$ ,  $F \in \mathbb{R}^{n-m}$ ) is flat, iff, exist  $\alpha \in \mathbb{N}$  and  $h(x, \dots, x^{(\alpha)}) \in \mathbb{R}^m$  such that the **generic** solution of

$$F(x, \dots, x^{(r)}) = 0, \quad y = h(x, \dots, x^{(\alpha)}) \quad \text{reads} \quad x = \mathcal{A}(y, \dots, y^{(\beta)})$$

$y$  is called a **flat output**: Fliess and co-workers 1991, ...

**Integrable** under-determined differential systems: Monge (1784), Darboux, Goursat, Hilbert (1912), Cartan (1914).

## Flat systems (Fliess-et-al, 1992,...,1999)

A basic definition extending remark of Isidori-Moog-DeLuca (CDC86) on dynamic feedback linearization (Charlet-Lévine-Marino (1989)):

$$\frac{d}{dt}x = f(x, u)$$

is flat, iff, exist  $m = \dim(u)$  output functions  $y = h(x, u, \dots, u^{(p)})$ ,  $\dim(h) = \dim(u)$ , such that the inverse of  $u \mapsto y$  has no dynamics, i.e.,

$$x = \Lambda \left( y, \dot{y}, \dots, y^{(q)} \right), \quad u = \Upsilon \left( y, \dot{y}, \dots, y^{(q+1)} \right).$$

Behind this: an equivalence relationship exchanging trajectories (absolute equivalence of Cartan and dynamic feedback: Shadwick (1990), Sluis (1992), Nieuwstadt-et-al (1994), Pomet et al (1992), Pomet (1995),... Lévine (2011) ).

## Equivalence and flatness (intrinsic point of view, IEEE-AC 1999)

Take  $\frac{d}{dt}x = f(x, u)$ ,  $(x, u) \in X \times U \subset \mathbb{R}^n \times \mathbb{R}^m$ . It generates a system  $(F, \mathfrak{M})$ , (D-variety) where

$$\mathfrak{M} := X \times U \times \mathbb{R}_m^\infty$$

with the vector field  $F(x, u, u^1, \dots) := (f(x, u), u^1, u^2, \dots)$ .  
 $(F, \mathfrak{M})$  is equivalent to  $(G, \mathfrak{N})$  ( $\dot{z} = g(z, v)$ :  $\mathfrak{N} := Z \times V \times \mathbb{R}_m^\infty$   
with the vector field  $G(z, v, v^1, \dots) := (g(z, v), v^1, v^2, \dots)$ ) iff  
exists an invertible transformation  $\Phi : \mathfrak{M} \rightarrow \mathfrak{N}$  such that

$$\forall \xi := (x, u, u^1, \dots) \in \mathfrak{M}, \quad G(\Phi(\xi)) = D\Phi(\xi) \cdot F(\xi).$$

## Equivalence and flatness (extrinsic point of view)

Elimination of  $u$  from the  $n$  state equations  $\frac{d}{dt}x = f(x, u)$  provides an under-determinate system of  $n - m$  equations with  $n$  unknowns

$$F\left(x, \frac{d}{dt}x\right) = 0.$$

An endogenous transformation  $x \mapsto z$  is defined by

$$z = \Phi(x, \dot{x}, \dots, x^{(p)}), \quad x = \Psi(z, \dot{z}, \dots, z^{(q)})$$

(nonlinear analogue of uni-modular matrices, the "integral free" transformations of Hilbert).

Two systems are equivalent, iff, exists an endogenous transformation exchanging the equations.

A system equivalent to the trivial equation  $z_1 = 0$  with  $z = (z_1, z_2)$  is flat with  $z_2$  the flat output.

## The time dependent definition

We present here the simplest version of this definition (Murray and co-workers (SIAM JCO 1998)):

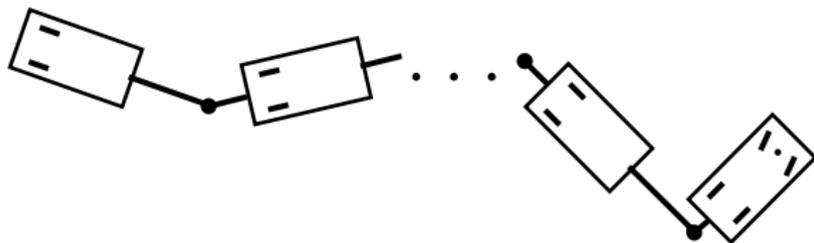
$$\frac{d}{dt}x = f(t, x, u)$$

is flat, iff, exist  $m = \dim(u)$  output functions

$y = h(t, x, u, \dots, u^{(p)})$ ,  $\dim(h) = \dim(u)$ , such that the inverse of  $u \mapsto y$  has no dynamics, i.e.,

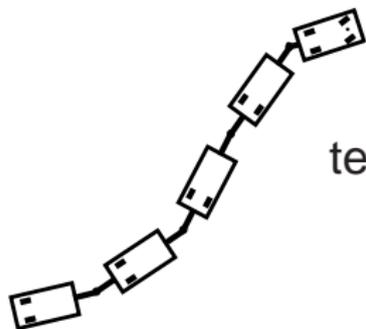
$$x = \Lambda \left( t, y, \dot{y}, \dots, y^{(q)} \right), \quad u = \Upsilon \left( t, y, \dot{y}, \dots, y^{(q+1)} \right).$$

The general  $n$ -trailer system for  $n \geq 2$  is not flat.

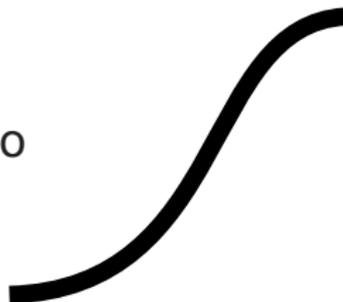


Proof: by pure chance, the characterization of codimension 2 contact systems is also a characterization of driftless flat systems (Cartan 1914, Martin-R. 1994) (adding integrator, endogenous or exogenous or singular dynamic feedbacks are useless here).

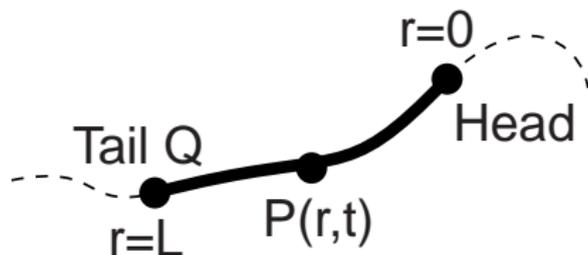
When the number  $n$  of trailers becomes large...



tends to



The nonholonomic snake: a trivial delay system.



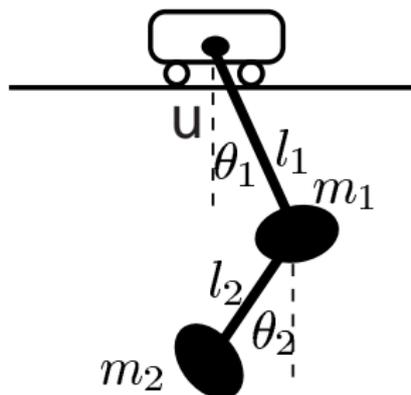
Implicit partial differential nonlinear system:

$$\left\| \frac{\partial P}{\partial r} \right\| = 1, \quad \frac{\partial P}{\partial r} \wedge \frac{\partial P}{\partial t} = 0.$$

General solution via  $s \mapsto Q(s)$  arbitrary smooth:

$$P(r, t) = Q(s(t) + L - r) \equiv \sum_{k \geq 0} \frac{(L - r)^k}{k!} \frac{dQ^k}{ds^k}(s(t)).$$

## Two linearized pendulum in series

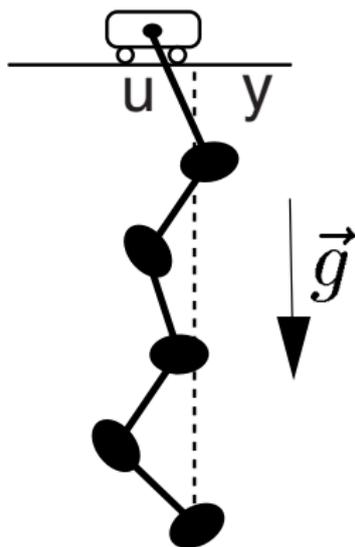


Flat output  $y = u + l_1\theta_1 + l_2\theta_2$ :

$$\theta_2 = -\frac{\ddot{y}}{g}, \quad \theta_1 = -\frac{m_1 \overbrace{(y - l_2\theta_2)}{\ddot{y}}}{(m_1 + m_2)g} + \frac{m_2}{m_1 + m_2}\theta_2$$

and  $u = y - l_1\theta_1 - l_2\theta_2$  is a linear combination of  $(y, y^{(2)}, y^{(4)})$ .

## $n$ pendulum in series

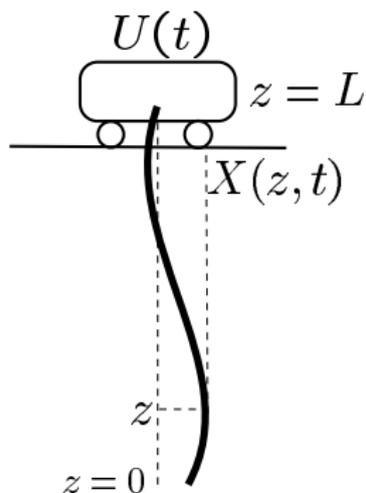


Flat output  $y = u + l_1\theta_1 + \dots + l_n\theta_n$ :

$$u = y + a_1y^{(2)} + a_2y^{(4)} + \dots + a_ny^{(2n)}.$$

When  $n$  tends to  $\infty$  the system tends to a partial differential equation.

## The heavy chain <sup>5</sup>



$$\frac{\partial^2 X}{\partial t^2} = \frac{\partial}{\partial z} \left( gz \frac{\partial X}{\partial z} \right)$$
$$X(L, t) = U(t)$$

Flat output  $y(t) = X(0, t)$  with

$$U(t) = \frac{1}{2\pi} \int_0^{2\pi} y \left( t - 2\sqrt{L/g} \sin \zeta \right) d\zeta$$

<sup>5</sup>N. Petit, P. R.: motion planning for heavy chain systems. SIAM J. Control and Optim., 41:475-495, 2001.

With the same flat output, for a discrete approximation ( $n$  pendulums in series,  $n$  large) we have

$$u(t) = y(t) + a_1 \ddot{y}(t) + a_2 y^{(4)}(t) + \dots + a_n y^{(2n)}(t),$$

for a continuous approximation (the heavy chain) we have

$$U(t) = \frac{1}{2\pi} \int_0^{2\pi} y\left(t + 2\sqrt{L/g} \sin \zeta\right) d\zeta.$$

Why? Because formally

$$y\left(t + 2\sqrt{L/g} \sin \zeta\right) = y(t) + \dots + \frac{\left(2\sqrt{L/g} \sin \zeta\right)^n}{n!} y^{(n)}(t) + \dots$$

But integral formula is preferable (divergence of the series...).

The general solution of the PDE

$$\frac{\partial^2 X}{\partial t^2} = \frac{\partial}{\partial z} \left( gz \frac{\partial X}{\partial z} \right)$$

is

$$X(z, t) = \frac{1}{2\pi} \int_0^{2\pi} y \left( t - 2\sqrt{z/g} \sin \zeta \right) d\zeta$$

where  $t \mapsto y(t)$  is any time function.

Proof: replace  $\frac{d}{dt}$  by  $s$ , the Laplace variable, to obtain a singular second order ODE in  $z$  with bounded solutions. Symbolic computations and operational calculus on

$$s^2 X = \frac{\partial}{\partial z} \left( gz \frac{\partial X}{\partial z} \right).$$

Symbolic computations in the Laplace domain

Thanks to  $x = 2\sqrt{\frac{z}{g}}$ , we get

$$x \frac{\partial^2 X}{\partial x^2}(x, t) + \frac{\partial X}{\partial x}(x, t) - x \frac{\partial^2 X}{\partial t^2}(x, t) = 0.$$

Use Laplace transform of  $X$  with respect to the variable  $t$

$$x \frac{\partial^2 \hat{X}}{\partial x^2}(x, s) + \frac{\partial \hat{X}}{\partial x}(x, s) - xs^2 \hat{X}(x, s) = 0.$$

This is a the Bessel equation defining  $J_0$  and  $Y_0$ :

$$\hat{X}(z, s) = A(s) J_0(2\iota s \sqrt{z/g}) + B(s) Y_0(2\iota s \sqrt{z/g}).$$

Since we are looking for a bounded solution at  $z = 0$  we have  $B(s) = 0$  and (remember that  $J_0(0) = 1$ ):

$$\hat{X}(z, s) = J_0(2\iota s \sqrt{z/g}) \hat{X}(0, s).$$

$$\hat{X}(z, s) = J_0(2s\sqrt{z/g})\hat{X}(0, s).$$

Using Poisson's integral representation of  $J_0$

$$J_0(\zeta) = \frac{1}{2\pi} \int_0^{2\pi} \exp(i\zeta \sin \theta) d\theta, \quad \zeta \in \mathbb{C}$$

we have

$$J_0(2s\sqrt{x/g}) = \frac{1}{2\pi} \int_0^{2\pi} \exp(2s\sqrt{x/g} \sin \theta) d\theta.$$

In terms of Laplace transforms, this last expression is a combination of delay operators:

$$X(z, t) = \frac{1}{2\pi} \int_0^{2\pi} y(t + 2\sqrt{z/g} \sin \theta) d\theta$$

with  $y(t) = X(0, t)$ .

## Explicit parameterization of the heavy chain

The general solution of

$$\frac{\partial^2 X}{\partial t^2} = \frac{\partial}{\partial z} \left( gz \frac{\partial X}{\partial z} \right), \quad U(t) = X(L, t)$$

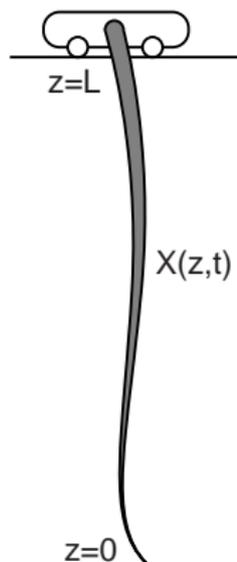
reads

$$X(z, t) = \frac{1}{2\pi} \int_0^{2\pi} y(t + 2\sqrt{z/g} \sin \theta) d\theta$$

There is a one to one correspondence between the (smooth) solutions of the PDE and the (smooth) functions  $t \mapsto y(t)$ .

## Heavy chain with a variable section

$$\left\{ \begin{array}{l} \frac{\tau'(z)}{g} \frac{\partial^2 X}{\partial t^2} = \frac{\partial}{\partial z} \left( \tau(z) \frac{\partial X}{\partial z} \right) \\ X(L, t) = u(t) \end{array} \right.$$



The general solution of

$$\left\{ \begin{array}{l} \frac{\tau'(z)}{g} \frac{\partial^2 X}{\partial t^2} = \frac{\partial}{\partial z} \left( \tau(z) \frac{\partial X}{\partial z} \right) \\ X(L, t) = u(t) \end{array} \right.$$

where  $\tau(z) \geq 0$  is the tension in the rope, can be parameterized by an arbitrary time function  $y(t)$ , the position of the free end of the system  $y = X(0, t)$ , via delay and advance operators with compact support.

## Sketch of the proof.

Main difficulty:  $\tau(0) = 0$ . The bounded solution  $B(z, s)$  of

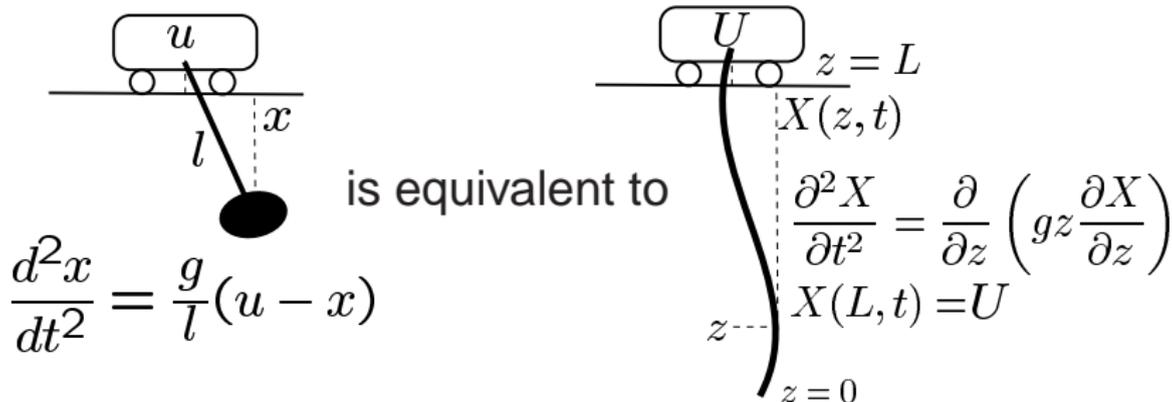
$$\frac{\partial}{\partial z} \left( \tau(z) \frac{\partial X}{\partial z} \right) = \frac{s^2 \tau'(z)}{g} X$$

is an entire function of  $s$ , is of exponential type and

$$\mathbb{R} \ni \omega \mapsto B(z, i\omega)$$

is  $L^2$  modulo some  $J_0$ . By the Paley-Wiener theorem  $B(z, s)$  can be described via

$$\int_a^b K(z, \zeta) \exp(s\zeta) d\zeta.$$



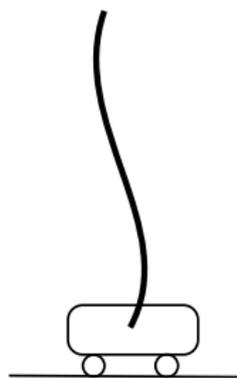
The following maps exchange the trajectories:

$$\begin{cases} x(t) = X(0, t) \\ u(t) = \frac{\partial^2 X}{\partial t^2}(0, t) \end{cases} \begin{cases} X(z, t) = \frac{1}{2\pi} \int_0^{2\pi} x \left( t - 2\sqrt{z/g} \sin \zeta \right) d\zeta \\ U(t) = \frac{1}{2\pi} \int_0^{2\pi} x \left( t - 2\sqrt{L/g} \sin \zeta \right) d\zeta \end{cases}$$

## The Indian rope.

$$\frac{\partial}{\partial z} \left( gz \frac{\partial X}{\partial z} \right) + \frac{\partial^2 X}{\partial t^2} = 0$$

$$X(L, t) = U(t)$$



The equation becomes elliptic and the Cauchy problem is not well posed in the sense of Hadamard. Nevertheless formulas are still valid with a complex time and  $y$  holomorphic

$$X(z, t) = \frac{1}{2\pi} \int_0^{2\pi} y \left( t - (2\sqrt{z/g} \sin \zeta) \sqrt{-1} \right) d\zeta.$$

## A computation due to Holmgren<sup>6</sup>

Take the 1D-heat equation,  $\frac{\partial \theta}{\partial t}(x, t) = \frac{\partial^2 \theta}{\partial x^2}(x, t)$  for  $x \in [0, 1]$  and set, **formally**,  $\theta = \sum_{i=0}^{\infty} a_i(t) \frac{x^i}{i!}$ . Since,

$$\frac{\partial \theta}{\partial t} = \sum_{i=0}^{\infty} \frac{da_i}{dt} \left( \frac{x^i}{i!} \right), \quad \frac{\partial^2 \theta}{\partial x^2} = \sum_{i=0}^{\infty} a_{i+2} \left( \frac{x^i}{i!} \right)$$

the heat equation  $\frac{\partial \theta}{\partial t} = \frac{\partial^2 \theta}{\partial x^2}$  reads  $\frac{d}{dt} a_i = a_{i+2}$  and thus

$$a_{2i+1} = a_1^{(i)}, \quad a_{2i} = a_0^{(i)}$$

With two **arbitrary smooth time-functions**  $f(t)$  and  $g(t)$ , playing the role of  $a_0$  and  $a_1$ , the general solution reads:

$$\theta(x, t) = \sum_{i=0}^{\infty} f^{(i)}(t) \left( \frac{x^{2i}}{(2i)!} \right) + g^{(i)}(t) \left( \frac{x^{2i+1}}{(2i+1)!} \right).$$

### Convergence issues ?

<sup>6</sup>E. Holmgren, Sur l'équation de la propagation de la chaleur. Arkiv für Math. Astr. Physik, t. 4, (1908), p. 1-4

# Gevrey functions<sup>7</sup>

- ▶ A  $C^\infty$ -function  $[0, T] \ni t \mapsto f(t)$  is of **Gevrey-order**  $\alpha$  when,  
 $\exists M, A > 0, \quad \forall t \in [0, T], \forall i \geq 0, \quad |f^{(i)}(t)| \leq MA^i \Gamma(1 + \alpha i)$

where  $\Gamma$  is the gamma function with  $n! = \Gamma(n + 1), \forall n \in \mathbb{N}$ .

- ▶ Analytic functions correspond to Gevrey-order  $\leq 1$ .
- ▶ When  $\alpha > 1$ , the set of  $C^\infty$ -functions with Gevrey-order  $\alpha$  contains **non-zero functions with compact supports**.

Prototype of such functions:

$$t \mapsto f(t) = \begin{cases} \exp\left(-\left(\frac{1}{t(1-t)}\right)^{\frac{1}{\alpha-1}}\right) & \text{if } t \in ]0, 1[ \\ 0 & \text{otherwise.} \end{cases}$$

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<sup>7</sup>M. Gevrey: La nature analytique des solutions des équations aux dérivées partielles, Ann. Sc. Ecole Norm. Sup., vol.25, pp:129–190, 1918. 

## Gevrey functions and exponential decay<sup>8</sup>

- ▶ Take, in the complex plane, the open bounded sector  $\mathcal{S}$  whose vertex is the origin. Assume that  $f$  is analytic on  $\mathcal{S}$  and admits an **exponential decay** of order  $\sigma > 0$  and type  $A$  in  $\mathcal{S}$ :

$$\exists C, \rho > 0, \quad \forall z \in \mathcal{S}, \quad |f(z)| \leq C|z|^\rho \exp\left(\frac{-1}{A|z|^\sigma}\right)$$

Then in any closed sub-sector  $\tilde{\mathcal{S}}$  of  $\mathcal{S}$  with origin as vertex, exists  $M > 0$  such that

$$\forall z \in \tilde{\mathcal{S}} \setminus \{0\}, \quad |f^{(i)}(z)| \leq MA^i \Gamma\left(1 + i\left(\frac{1}{\sigma} + 1\right)\right)$$

- ▶ **Rule of thumb**: if a piece-wise analytic  $f$  admits an exponential decay of order  $\sigma$  then it is of Gevrey-order  $\alpha = \frac{1}{\sigma} + 1$ .

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<sup>8</sup>J.P. Ramis: *Déviage Gevrey*. Astérisque, vol:59-60, pp:173–204, 1978.

See also J.P. Ramis: *Séries Divergentes et Théories Asymptotiques*; SMF, Panoramas et Synthèses, 1993.

## Gevrey space and ultra-distributions<sup>9</sup>

Denote by  $\mathcal{D}_\alpha$  the set of functions  $\mathbb{R} \mapsto \mathbb{R}$  of order  $\alpha > 1$  and with compact supports. As for the class of  $C^\infty$  functions, **most of the usual manipulations remain in  $\mathcal{D}_\alpha$** :

- ▶  $\mathcal{D}_\alpha$  is stable by addition, multiplication, derivation, integration, ....
- ▶ if  $f \in \mathcal{D}_\alpha$  and  $F$  is an analytic function on the image of  $f$ , then  $F(f)$  remains in  $\mathcal{D}_\alpha$ .
- ▶ if  $f \in \mathcal{D}_\alpha$  and  $F \in L^1_{loc}(\mathbb{R})$  then the convolution  $f * F$  is of Gevrey-order  $\alpha$  on any compact interval.

As for the construction of  $\mathcal{D}'$ , the space of distributions (the dual of  $\mathcal{D}$  the space of  $C^\infty$  functions of compact supports), one can construct  $\mathcal{D}'_\alpha \supset \mathcal{D}'$ , a space of **ultra-distributions**, the dual of  $\mathcal{D}_\alpha \subset \mathcal{D}$ .

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<sup>9</sup>See, e.g., I.M. Guelfand and G.E. Chilov: Les Distributions, tomes 2 et 3. Dunod, Paris, 1964.

## Symbolic computations: $s := d/dt$ , $s \in \mathbb{C}$

The general solution of  $\theta'' = s\theta$  reads ( $' := d/dx$ )

$$\theta = \cosh(x\sqrt{s}) f(s) + \frac{\sinh(x\sqrt{s})}{\sqrt{s}} g(s)$$

where  $f(s)$  and  $g(s)$  are the two constants of integration. Since  $\cosh$  and  $\sinh$  gather the even and odd terms of the series defining  $\exp$ , we have

$$\cosh(x\sqrt{s}) = \sum_{i \geq 0} s^i \frac{x^{2i}}{(2i)!}, \quad \frac{\sinh(x\sqrt{s})}{\sqrt{s}} = \sum_{i \geq 0} s^i \frac{x^{2i+1}}{(2i+1)!}$$

and we recognize  $\theta = \sum_{i=0}^{\infty} f^{(i)}(t) \left( \frac{x^{2i}}{(2i)!} \right) + g^{(i)}(t) \left( \frac{x^{2i+1}}{(2i+1)!} \right)$ .

For each  $x$ , the operators  $\cosh(x\sqrt{s})$  and  $\sinh(x\sqrt{s})/\sqrt{s}$  are **ultra-distributions** of  $\mathcal{D}'_{2-}$ :

$$\sum_{i \geq 0} \frac{(-1)^i x^{2i}}{(2i)!} \delta^{(i)}(t), \quad \sum_{i \geq 0} \frac{(-1)^i x^{2i+1}}{(2i+1)!} \delta^{(i)}(t)$$

with  $\delta$ , the Dirac distribution.

## Entire functions of $s = d/dt$ as ultra-distributions

- ▶  $\mathbb{C} \ni s \mapsto P(s) = \sum_{i \geq 0} a_i s^i$  is an entire function when the radius of convergence is infinite.
- ▶ If its **order at infinity** is  $\sigma > 0$  and its type is finite, i.e.,  $\exists M, K > 0$  such that  $\forall s \in \mathbb{C}, |P(s)| \leq M \exp(K|s|^\sigma)$ , then

$$\exists A, B > 0 \mid \forall i \geq 0, \quad |a_i| \leq A \frac{B^i}{\Gamma(i/\sigma + 1)}.$$

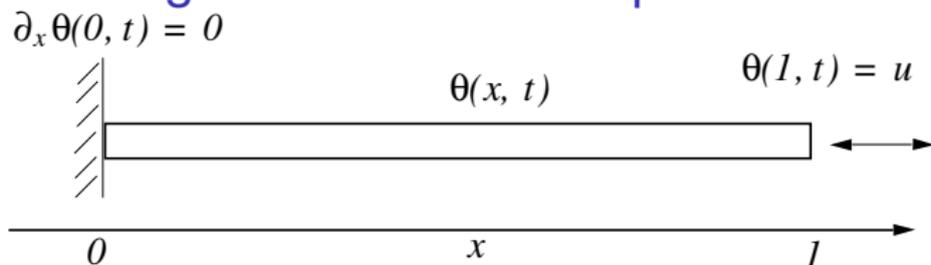
$\cosh(\sqrt{s})$  and  $\sinh(\sqrt{s})/\sqrt{s}$  are entire functions of order  $\sigma = 1/2$  and of type 1.

- ▶ Take  $P(s)$  of order  $\sigma < 1$  with  $s = d/dt$ . Then  $P \in \mathcal{D}'_{\frac{1}{\sigma}-}$ :  $P(s)f(s)$  corresponds, in the time domain, to **absolutely convergent series**

$$P(s)y(s) \equiv \sum_{i=0}^{\infty} a_i f^{(i)}(t)$$

when  $t \mapsto f(t)$  is a  $C^\infty$ -function of **Gevrey-order**  $\alpha < 1/\sigma$ .

# Motion planning for the 1D heat equation



The data are:

1. the model relating the control input  $u(t)$  to the state,  $(\theta(x, t))_{x \in [0, 1]}$ :

$$\frac{\partial \theta}{\partial t}(x, t) = \frac{\partial^2 \theta}{\partial x^2}(x, t), \quad x \in [0, 1]$$

$$\frac{\partial \theta}{\partial x}(0, t) = 0 \quad \theta(1, t) = u(t).$$

2. A transition time  $T > 0$ , the initial (resp. final) state:  
 $[0, 1] \ni x \mapsto p(x)$  (resp.  $q(x)$ )

The goal is to find the **open-loop control**  $[0, T] \ni t \mapsto u(t)$  steering  $\theta(x, t)$  from the initial profile  $\theta(x, 0) = p(x)$  to the final profile  $\theta(x, T) = q(x)$ .

## Series solutions

Set, formally

$$\theta = \sum_{i=0}^{\infty} a_i(t) \frac{x^i}{i!}, \quad \frac{\partial \theta}{\partial t} = \sum_{i=0}^{\infty} \frac{da_i}{dt} \left( \frac{x^i}{i!} \right), \quad \frac{\partial^2 \theta}{\partial x^2} = \sum_{i=0}^{\infty} a_{i+2} \left( \frac{x^i}{i!} \right)$$

and  $\frac{\partial \theta}{\partial t} = \frac{\partial^2 \theta}{\partial x^2}$  reads  $\frac{d}{dt} a_i = a_{i+2}$ . Since  $a_1 = \frac{\partial \theta}{\partial x}(0, t) = 0$  and  $a_0 = \theta(0, t)$  we have

$$a_{2i+1} = 0, \quad a_{2i} = a_0^{(i)}$$

Set  $y := a_0 = \theta(0, t)$  we have, in the time domain,

$$\theta(x, t) = \sum_{i=0}^{\infty} \left( \frac{x^{2i}}{(2i)!} \right) y^{(i)}(t), \quad u(t) = \sum_{i=0}^{\infty} \left( \frac{1}{(2i)!} \right) y^{(i)}(t)$$

that also reads in the Laplace domain ( $s = d/dt$ ):

$$\theta(x, s) = \cosh(x\sqrt{s}) y(s), \quad u(s) = \cosh(\sqrt{s}) y(s).$$

## An explicit parameterization of trajectories

For any  $C^\infty$ -function  $y(t)$  of Gevrey-order  $\alpha < 2$ , the time function

$$u(t) = \sum_{i=1}^{+\infty} \frac{y^{(i)}(t)}{(2i)!}$$

is well defined and smooth. The  $(x, t)$ -function

$$\theta(x, t) = \sum_{i=1}^{+\infty} \frac{y^{(i)}(t)}{(2i)!} x^{2i}$$

is also well defined (entire versus  $x$  and smooth versus  $t$ ). Moreover for all  $t$  and  $x \in [0, 1]$ , we have, whatever  $t \mapsto y(t)$  is,

$$\frac{\partial \theta}{\partial t}(x, t) = \frac{\partial^2 \theta}{\partial x^2}(x, t), \quad \frac{\partial \theta}{\partial x}(0, t) = 0, \quad \theta(1, t) = u(t)$$

An infinite dimensional analogue of differential flatness.<sup>10</sup>

<sup>10</sup>Fliess et al: Flatness and defect of nonlinear systems: introductory theory and examples, International Journal of Control. vol.61, pp:1327-1361. 1995.

## Motion planning of the heat equation<sup>11</sup>

Take  $\sum_{i \geq 0} a_i \frac{\xi^i}{i!}$  and  $\sum_{i \geq 0} b_i \frac{\xi^i}{i!}$  entire functions of  $\xi$ . With  $\sigma > 1$

$$y(t) = \left( \sum_{i \geq 0} a_i \frac{t^i}{i!} \right) \left( \frac{e^{-\frac{T^\sigma}{(T-t)^\sigma}}}{e^{-\frac{T^\sigma}{t^\sigma}} + e^{-\frac{T^\sigma}{(T-t)^\sigma}} \right) + \left( \sum_{i \geq 0} b_i \frac{t^i}{i!} \right) \left( \frac{e^{-\frac{T^\sigma}{t^\sigma}}}{e^{-\frac{T^\sigma}{t^\sigma}} + e^{-\frac{T^\sigma}{(T-t)^\sigma}} \right)$$

the series

$$\theta(x, t) = \sum_{i=1}^{+\infty} \frac{y^{(i)}(t)}{(2i)!} x^{2i}, \quad u(t) = \sum_{i=1}^{+\infty} \frac{y^{(i)}(t)}{(2i)!}.$$

are convergent and provide a trajectory from

$$\theta(x, 0) = \sum_{i \geq 0} a_i \frac{x^{2i}}{(2i)!} \quad \text{to} \quad \theta(x, T) = \sum_{i \geq 0} b_i \frac{x^{2i}}{(2i)!}$$

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<sup>11</sup>B. Laroche, Ph. Martin, P. R.: Motion planning for the heat equation. Int. Journal of Robust and Nonlinear Control. Vol.10, pp:629–643, 2000. 

# Real-time motion planning for the heat equation

Take  $\sigma > 1$  and  $\epsilon > 0$ . Consider the positive function

$$\phi_\epsilon(t) = \frac{\exp\left(\frac{-\epsilon^{2\sigma}}{(-t(t+\epsilon))^\sigma}\right)}{A_\epsilon} \quad \text{for } t \in [-\epsilon, 0]$$

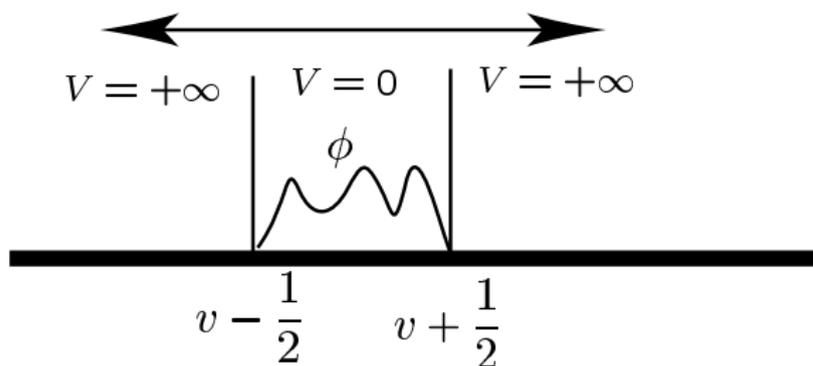
prolonged by 0 outside  $[-\epsilon, 0]$  and where the normalization constant  $A_\epsilon > 0$  is such that  $\int \phi_\epsilon = 1$ .

For any  $L^1_{loc}$  signal  $t \mapsto Y(t)$ , set  $y_r = \phi_\epsilon * Y$ : its order  $1 + 1/\sigma$  is less than 2. Then  $\theta_r = \cosh(x\sqrt{s})y_r$  reads

$$\theta_r(x, t) = \Phi_{x,\epsilon} * Y(t), \quad u_r(t) = \Phi_{1,\epsilon} * Y(t),$$

where for each  $x$ ,  $\Phi_{x,\epsilon} = \cosh(x\sqrt{s})\phi_\epsilon$  is a smooth time function with support contained in  $[-\epsilon, 0]$ . Since  $u_r(t)$  and the profile  $\theta_r(\cdot, t)$  depend only on the values of  $Y$  on  $[t - \epsilon, t]$ , such computations are well adapted to **real-time generation of reference trajectories**  $t \mapsto (\theta_r, u_r)$  (see matlab code `heat.m`).

# Quantum particle inside a moving box<sup>12</sup>



Schrödinger equation in a Galilean frame:

$$i \frac{\partial \phi}{\partial t} = -\frac{1}{2} \frac{\partial^2 \phi}{\partial z^2}, \quad z \in \left[ v - \frac{1}{2}, v + \frac{1}{2} \right],$$
$$\phi\left(v - \frac{1}{2}, t\right) = \phi\left(v + \frac{1}{2}, t\right) = 0$$

<sup>12</sup>P.R.: Control of a quantum particle in a moving potential well. IFAC 2nd Workshop on Lagrangian and Hamiltonian Methods for Nonlinear Control, 2003. See, for the proof of nonlinear controllability, K. Beauchard and J.-M. Coron: Controllability of a quantum particle in a moving potential well; J. of Functional Analysis, vol.232, pp:328–389, 2006.

# Particle in a moving box of position $v$

- ▶ In a Galilean frame

$$i \frac{\partial \phi}{\partial t} = -\frac{1}{2} \frac{\partial^2 \phi}{\partial z^2}, \quad z \in [v - \frac{1}{2}, v + \frac{1}{2}],$$
$$\phi(v - \frac{1}{2}, t) = \phi(v + \frac{1}{2}, t) = 0$$

where  $v$  is the position of the box and  $z$  is an absolute position.

- ▶ In the box frame  $x = z - v$ :

$$i \frac{\partial \psi}{\partial t} = -\frac{1}{2} \frac{\partial^2 \psi}{\partial x^2} + \ddot{v} x \psi, \quad x \in [-\frac{1}{2}, \frac{1}{2}],$$
$$\psi(-\frac{1}{2}, t) = \psi(\frac{1}{2}, t) = 0$$

## Tangent linearization around state $\bar{\psi}$ of energy $\bar{\omega}$

With<sup>13</sup>  $-\frac{1}{2} \frac{\partial^2 \bar{\psi}}{\partial x^2} = \bar{\omega} \bar{\psi}$ ,  $\bar{\psi}(-\frac{1}{2}) = \bar{\psi}(\frac{1}{2}) = 0$  and with

$$\psi(x, t) = \exp(-i\bar{\omega}t)(\bar{\psi}(x) + \Psi(x, t))$$

$\Psi$  satisfies

$$i \frac{\partial \Psi}{\partial t} + \bar{\omega} \Psi = -\frac{1}{2} \frac{\partial^2 \Psi}{\partial x^2} + \ddot{v}x(\bar{\psi} + \Psi)$$
$$0 = \Psi(-\frac{1}{2}, t) = \Psi(\frac{1}{2}, t).$$

Assume  $\Psi$  and  $\ddot{v}$  small and neglecte the second order term  $\ddot{v}x\Psi$ :

$$i \frac{\partial \Psi}{\partial t} + \bar{\omega} \Psi = -\frac{1}{2} \frac{\partial^2 \Psi}{\partial x^2} + \ddot{v}x\bar{\psi}, \quad \Psi(-\frac{1}{2}, t) = \Psi(\frac{1}{2}, t) = 0.$$

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<sup>13</sup>Remember that  $\int_{-1/2}^{1/2} \bar{\psi}^2(x) dx = 1$ .

## Operational computations $s = d/dt$

The general solution of ( $'$  stands for  $d/dx$ )

$$(\iota s + \bar{\omega})\Psi = -\frac{1}{2}\Psi'' + s^2 v x \bar{\psi}$$

is

$$\Psi = A(s, x)a(s) + B(s, x)b(s) + C(s, x)v(s)$$

where

$$A(s, x) = \cos\left(x\sqrt{2\iota s + 2\bar{\omega}}\right)$$

$$B(s, x) = \frac{\sin\left(x\sqrt{2\iota s + 2\bar{\omega}}\right)}{\sqrt{2\iota s + 2\bar{\omega}}}$$

$$C(s, x) = (-\iota s x \bar{\psi}(x) + \bar{\psi}'(x)).$$

## Case $x \mapsto \bar{\phi}(x)$ even

The boundary conditions imply

$$A(s, 1/2)a(s) = 0, \quad B(s, 1/2)b(s) = -\bar{\psi}'(1/2)v(s).$$

$a(s)$  is a torsion element: the system is not controllable.  
Nevertheless, for steady-state controllability, we have

$$b(s) = -\bar{\psi}'(1/2) \frac{\sin\left(\frac{1}{2}\sqrt{-2\imath s + 2\bar{\omega}}\right)}{\sqrt{-2\imath s + 2\bar{\omega}}} y(s)$$

$$v(s) = \frac{\sin\left(\frac{1}{2}\sqrt{2\imath s + 2\bar{\omega}}\right)}{\sqrt{2\imath s + 2\bar{\omega}}} \frac{\sin\left(\frac{1}{2}\sqrt{-2\imath s + 2\bar{\omega}}\right)}{\sqrt{-2\imath s + 2\bar{\omega}}} y(s)$$

$$\Psi(s, x) = B(s, x)b(s) + C(s, x)v(s)$$

# Series and convergence

$$v(s) = \frac{\sin\left(\frac{1}{2}\sqrt{2\imath s + 2\bar{\omega}}\right)}{\sqrt{2\imath s + 2\bar{\omega}}} \frac{\sin\left(\frac{1}{2}\sqrt{-2\imath s + 2\bar{\omega}}\right)}{\sqrt{-2\imath s + 2\bar{\omega}}} y(s) = F(s)y(s)$$

where the **entire function**  $s \mapsto F(s)$  is of **order 1/2**,

$$\exists K, M > 0, \forall s \in \mathbb{C}, \quad |F(s)| \leq K \exp(M|s|^{1/2}).$$

Set  $F(s) = \sum_{n \geq 0} a_n s^n$  where  $|a_n| \leq K^n / \Gamma(1 + 2n)$  with  $K > 0$  independent of  $n$ . Then  $F(s)y(s)$  corresponds, in the time domain, to

$$\sum_{n \geq 0} a_n y^{(n)}(t)$$

that is convergent when  $t \mapsto y(t)$  is  $C^\infty$  of **Gevrey-order**  $\alpha < 2$ .

# Steady state controllability

Steering from  $\Psi = 0$ ,  $v = 0$  at time  $t = 0$ , to  $\Psi = 0$ ,  $v = D$  at  $t = T$  is possible with the following  $C^\infty$ -function of Gevrey-order  $\sigma + 1$ :

$$[0, T] \ni t \mapsto y(t) = \begin{cases} 0 & \text{for } t \leq 0 \\ \bar{D} \frac{\exp\left(-\left(\frac{T}{t}\right)^{\frac{1}{\sigma}}\right)}{\exp\left(-\left(\frac{T}{t}\right)^{\frac{1}{\sigma}}\right) + \exp\left(-\left(\frac{T}{T-t}\right)^{\frac{1}{\sigma}}\right)} & \text{for } 0 < t < T \\ \bar{D} & \text{for } t \geq T \end{cases}$$

with  $\bar{D} = \frac{2\bar{\omega}D}{\sin^2(\sqrt{\bar{\omega}}/2)}$ . The fact that this  $C^\infty$ -function is of Gevrey-order  $\sigma + 1$  results from its exponential decay of order  $1/\sigma$  around 0 and  $T$ .

# Practical computations via Cauchy formula

Using the "magic" Cauchy formula

$$y^{(n)}(t) = \frac{\Gamma(n+1)}{2i\pi} \oint_{\gamma} \frac{y(t+\xi)}{\xi^{n+1}} d\xi$$

where  $\gamma$  is a closed path around zero,  $\sum_{n \geq 0} a_n y^{(n)}(t)$  becomes

$$\sum_{n \geq 0} a_n \frac{\Gamma(n+1)}{2i\pi} \oint_{\gamma} \frac{y(t+\xi)}{\xi^{n+1}} d\xi = \frac{1}{2i\pi} \oint_{\gamma} \left( \sum_{n \geq 0} a_n \frac{\Gamma(n+1)}{\xi^{n+1}} \right) y(t+\xi) d\xi.$$

But

$$\sum_{n \geq 0} a_n \frac{\Gamma(n+1)}{\xi^{n+1}} = \int_{D_\delta} F(s) \exp(-s\xi) ds = B_1(F)(\xi)$$

is the **Borel/Laplace transform** of  $F$  in direction  $\delta \in [0, 2\pi]$ .

## Practical computations via Cauchy formula (end)

(matlab code `Qbox.m`)

In the time domain  $F(s)y(s)$  corresponds to

$$\frac{1}{2i\pi} \oint_{\gamma} B_1(F)(\xi) y(t + \xi) d\xi$$

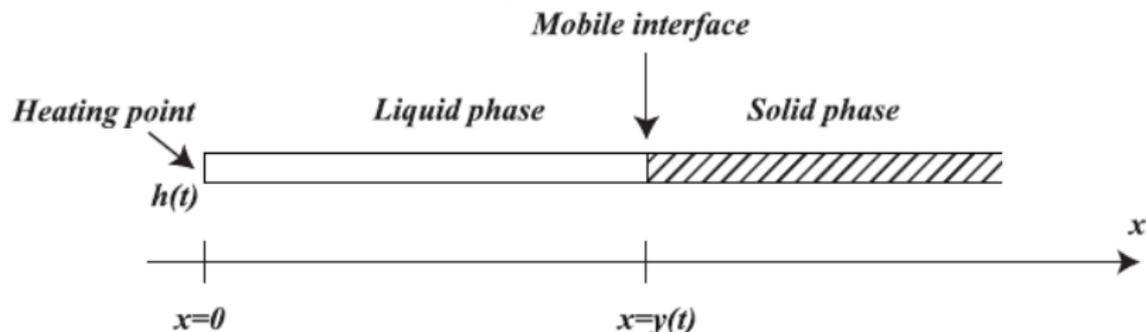
where  $\gamma$  is a closed path around zero. Such integral representation is very useful when  $y$  is defined by convolution with a real signal  $Y$ ,

$$y(\zeta) = \frac{1}{\varepsilon\sqrt{2\pi}} \int_{-\infty}^{+\infty} \exp(-(\zeta - t)^2/2\varepsilon^2) Y(t) dt$$

where  $\mathbb{R} \ni t \mapsto Y(t) \in \mathbb{R}$  is any measurable and bounded function. **Approximate** motion planning with:

$$v(t) = \int_{-\infty}^{+\infty} \left[ \frac{1}{i\varepsilon(2\pi)^{3/2}} \oint_{\gamma} B_1(F)(\xi) \exp(-(\xi - \tau)^2/2\varepsilon^2) d\xi \right] Y(t-\tau) d\tau.$$

# A free-boundary Stefan problem<sup>14</sup>



$$\frac{\partial \theta}{\partial t}(x, t) = \frac{\partial^2 \theta}{\partial x^2}(x, t) - \nu \frac{\partial \theta}{\partial x}(x, t) - \rho \theta^2(x, t), \quad x \in [0, y(t)]$$

$$\theta(0, t) = u(t), \quad \theta(y(t), t) = 0$$

$$\frac{\partial \theta}{\partial x}(y(t), t) = -\frac{d}{dt}y(t)$$

with  $\nu, \rho \geq 0$  parameters.

<sup>14</sup>W. Dunbar, N. Petit, P. R., Ph. Martin. Motion planning for a non-linear Stefan equation. ESAIM: Control, Optimisation and Calculus of Variations, 9:275–296, 2003.

## Series solutions

- ▶ Set  $\theta(x, t) = \sum_{i=0}^{\infty} a_i(t) \frac{(x-y(t))^i}{i!}$  in

$$\frac{\partial \theta}{\partial t}(x, t) = \frac{\partial^2 \theta}{\partial x^2}(x, t) - \nu \frac{\partial \theta}{\partial x}(x, t) - \rho \theta^2(x, t), \quad x \in [0, y(t)]$$

$$\theta(0, t) = u(t), \quad \theta(y(t), t) = 0, \quad \frac{\partial \theta}{\partial x}(y(t), t) = -\frac{d}{dt}y(t)$$

Then  $\frac{\partial \theta}{\partial t} = \frac{\partial^2 \theta}{\partial x^2}$  yields

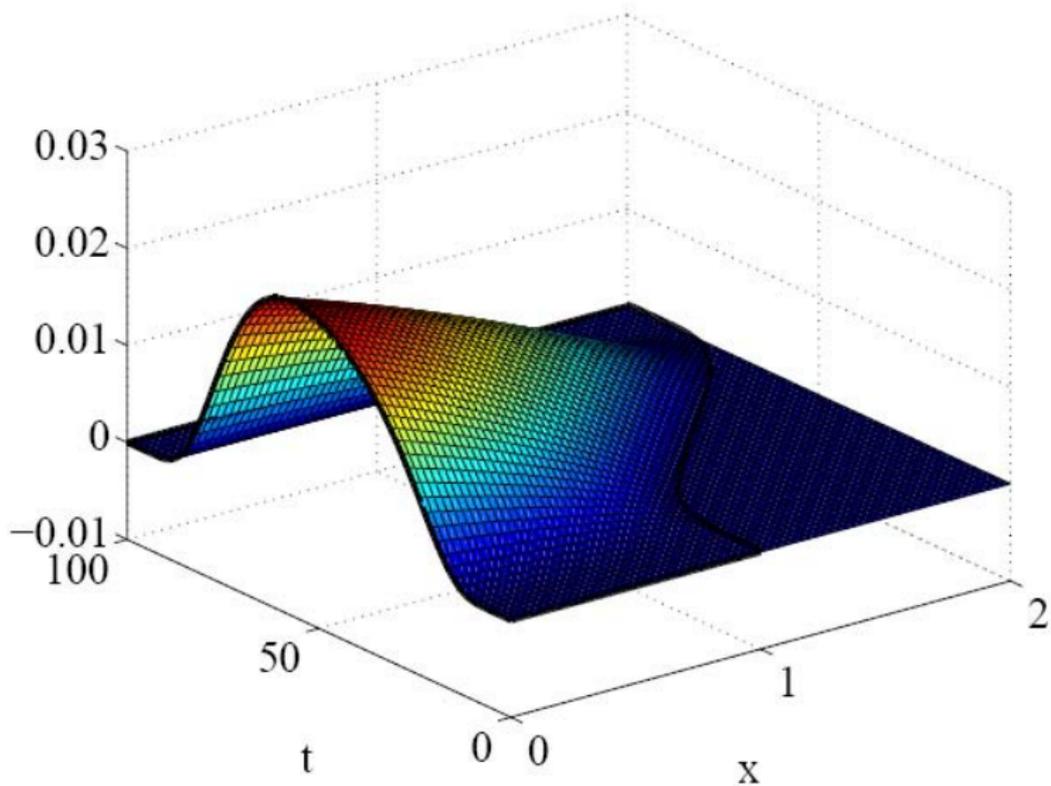
$$a_{i+2} = \frac{d}{dt}a_i - a_{i-1} \frac{d}{dt}y + \nu a_{i+1} + \rho \sum_{k=0}^i \binom{i}{k} a_{i-k} a_k$$

and the boundary conditions:  $a_0 = 0$  and  $a_1 = -\frac{d}{dt}y$ .

- ▶ The series defining  $\theta$  admits a strictly positive radius of convergence as soon as  $y$  is of Gevrey-order  $\alpha$  strictly less than 2.

## Growth of the liquide zone with $\theta \geq 0$

$\nu = 0.5$ ,  $\rho = 1.5$ ,  $y$  goes from 1 to 2.



## Conclusion for PDE

- ▶ For other 1D PDE of engineering interest with motion planning see the book of J. Rudolph: Flatness Based Control of Distributed Parameter Systems (Shaker-Germany, 2003)
- ▶ For tracking and feedback stabilization on linear 1D diffusion and wave equations, see the book of M. Krstić and A. Smyshlyaev : Boundary Control of PDEs: a Course on Backstepping Designs (SIAM, 2008).
- ▶ Open questions:
  - ▶ Combine **divergent series** and smallest-term summation (see the PhD of Th. Meurer: Feedforward and Feedback Tracking Control of Diffusion-Convection-Reaction Systems using Summability Methods (Stuttgart, 2005)).
  - ▶ **2D heat equation with a scalar control**  $u(t)$ : with modal decomposition and symbolic computations, we get  $u(s) = P(s)y(s)$  with  $P(s)$  an entire function (coding the spectrum) of order 1 but infinite type  $|P(s)| \leq M \exp(K|s| \log(|s|))$ . It yields **divergence series** for any  $C^\infty$  function  $y \neq 0$  with compact support.

## $u(s) = P(s)y(s)$ for 1D and 2D heat equations

- ▶ 1D heat equation: eigenvalue asymptotics  $\lambda_n \sim -n^2$ :

$$\text{Prototype: } P(s) = \prod_{n=1}^{+\infty} \left(1 - \frac{s}{n^2}\right) = \frac{\sinh(\pi\sqrt{s})}{\pi\sqrt{s}}$$

entire function of order  $1/2$ .

- ▶ 2D heat equation in a domain  $\Omega$  with a **single scalar control**  $u(t)$  on the boundary  $\partial\Omega_1$  ( $\partial\Omega = \partial\Omega_1 \cup \partial\Omega_2$ ):

$$\frac{\partial\theta}{\partial t} = \Delta\theta \text{ on } \Omega, \quad \theta = u(t) \text{ on } \partial\Omega_1, \quad \frac{\partial\theta}{\partial n} = 0 \text{ on } \partial\Omega_2$$

Eigenvalue asymptotics  $\lambda_n \sim -n$

$$\text{Prototype: } P(s) = \prod_{n=1}^{+\infty} \left(1 + \frac{s}{n}\right) \exp(-s/n) = \frac{\exp(-\gamma s)}{s\Gamma(s)}$$

entire function of order 1 but of infinite type<sup>15</sup>

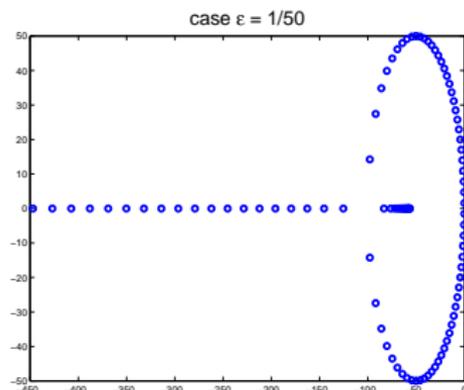
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<sup>15</sup>For the links between the distributions of the zeros and the order at infinity of entire functions see the book of B.Ja Levin: Distribution of Zeros of Entire Functions; AMS, 1972.

## Symbolic computations with Laplace variable $s = \frac{d}{dt}$

- ▶ **Wave 1D:**  $u = \cosh(s)y$ . General case is similar:  $u = P(s)y$  where the zeros of  $P$  are the eigen-values  $\pm i\omega_n$  with asymptotic  $\omega_n \sim n$ ;  $P(s)$  entire function of order 1 and finite type (in time domain: advance/delay operator with compact support).
- ▶ **Diffusion 1D:**  $u = \cosh(\sqrt{s})u$ . General case is similar:  $u = P(s)y$  where the zeros of  $P$  are the eigen-values  $-\lambda_n$  with asymptotic  $\lambda_n \sim n^2$ ;  $P(s)$  entire function of order 1/2 (in time domain: ultra-distribution made of an infinite sum of Dirac derivatives applied on Gevrey functions with compact support of order  $< 2$ ).
- ▶ **Wave 2D:** since  $\omega_n \sim \sqrt{n}$ ,  $P$  entire with order 2 but infinite type; prototype  $P(s) = \prod_{n=1}^{+\infty} \left(1 - \frac{s^2}{n}\right) \exp(s^2/n) = \frac{-\exp(\gamma s^2)}{s^2 \Gamma(-s^2)}$ .  
**Diffusion 2D:** since  $\lambda_n \sim -n$ ,  $P$  entire with order 1 but infinite type; prototype  $P(s) = \prod_{n=1}^{+\infty} \left(1 + \frac{s}{n}\right) \exp(-s/n) = \frac{\exp(-\gamma s)}{s \Gamma(s)}$ .  
**Open Question:** interpretation of  $P(s)$  in time domain as operator on a set of time functions  $y(t)$ ...

## Wave 1D with internal damping



$$\frac{\partial^2 H}{\partial t^2} = \frac{\partial^2 H}{\partial x^2} + \epsilon \frac{\partial^3 H}{\partial x^2 \partial t}$$

$$H(0, t) = 0, \quad H(1, t) = u(t)$$

where the eigenvalues are the zeros of

$$P(s) = \cosh \left( \frac{s}{\sqrt{\epsilon s + 1}} \right).$$

Approximate controllability depends on the functional space chosen to have a well-posed Cauchy problem<sup>16</sup>

<sup>16</sup>Rosier-R, CAO'06. 13th IFAC Workshop on Control Applications of Optimisation. 2006.

## Dispersive wave 1D (Maxwell-Lorentz)

Propagation of electro-magnetic wave in a partially transparent medium:

$$\frac{\partial^2}{\partial t^2}(E + D) = c^2 \frac{\partial^2}{\partial x^2} E, \quad \frac{\partial^2 D}{\partial t^2} = \omega_0^2(\epsilon E - D)$$

where  $\omega_0$  is associated to an adsorption ray and  $\epsilon$  is the coupling constant between medium of polarization  $P$  and travelling field  $E$

- ▶ The **eigenvalues** rely on the analytic function ( $s = d/dt$  Laplace variable,  $L$  length)

$$Q^\pm(s, L) = \exp\left(\pm \frac{Ls}{c} \sqrt{\left(1 + \frac{\epsilon s^2}{\omega_0^2 + s^2}\right)}\right)$$

The **essential singularity** in  $s = \pm i\omega_0$  yields an **accumulation** of eigenvalues around  $\pm\omega_0$ .

- ▶ Few works on this kind of PDE with spectrum that accumulates at finite distance.

## The flatness characterization problem

$\frac{d}{dt}x = f(x, u)$  is said  $r$ -flat if exists a flat output  $y$  only function of  $(x, u, \dot{u}, \dots, u^{(r-1)})$ ; 0-flat means  $y = h(x)$ .

Example:

$$x_1^{(\alpha_1)} = u_1, \quad x_2^{(\alpha_2)} = u_2, \quad \frac{d}{dt}x_3 = u_1 u_2$$

is  $[r := \min(\alpha_1, \alpha_2) - 1]$ -flat with

$$y_1 = x_3 + \sum_{i=1}^{\alpha_1} (-1)^i x_1^{(\alpha_1-i)} u_2^{(i-1)}, \quad y_2 = x_2,$$

**Conjecture:** there is no flat output depending on derivatives of  $u$  of order less than  $r - 1$ .

**The main difficulty:** for  $\frac{d}{dt}x = f(x, u)$  with  $y = h(x, u, \dots, u^{(p)})$  as flat output, we do not know an upper-bound on  $p$  with respect to  $n = \dim(x)$ ,  $m = \dim(u)$ ,  $\dots$

## Systems linearizable by static feedback

- ▶ A system which is linearizable by static feedback and coordinate change is flat: geometric necessary and sufficient conditions by Jakubczyk and Respondek (1980) (see also Hunt et al. (1983)).
- ▶ When there is only one control input, flatness reduces to static feedback linearizability (Charlet et al. (1989))

## Affine control systems of small co-dimension

- ▶ Affine systems of codimension 1.

$$\frac{d}{dt}x = f_0(x) + \sum_{j=1}^{n-1} u_j g_j(x), \quad x \in \mathbb{R}^n,$$

is 0-flat as soon as it is controllable, Charlet et al. (1989)

- ▶ Affine systems with 2 inputs and 4 states. Necessary and sufficient conditions for 1-flatness (Pomet (1997)) give a good idea of the complexity of checking  $r$ -flatness even for  $r$  small.

## Driftless systems with two controls.



$$\frac{d}{dt}x = f_1(x)u_1 + f_2(x)u_2$$

is flat if and only if the generic rank of  $E_k$  is equal to  $k + 2$  for  $k = 0, \dots, n - 2$  where

$$E_0 := \text{span}\{f_1, f_2\}$$

$$E_{k+1} := \text{span}\{E_k, [E_k, E_k]\}, \quad k \geq 0.$$

Proof: Martin and R. (1994) with a theorem of Cartan (1916) on Pfaffian systems.

- ▶ A flat two-input driftless system satisfying some additional regularity conditions (Murray (1994)) can be put into the *chained system*

$$\begin{aligned} \frac{d}{dt}x_1 &= u_1, & \frac{d}{dt}x_2 &= u_2 \\ \frac{d}{dt}x_3 &= x_2 u_1, & \dots, & \frac{d}{dt}x_n = x_{n-1} u_1. \end{aligned}$$

## Codimension 2 driftless systems



$$\frac{d}{dt}x = \sum_{i=1}^{n-2} u_i f_i(x), \quad x \in \mathbb{R}^n$$

is flat as soon as it is controllable (Martin and R. (1995))

- ▶ Tools: exterior differential systems.
- ▶ Many nonholonomic control systems are flat.

## The ruled-manifold criterion (R. (1995))

- ▶ Assume  $\dot{x} = f(x, u)$  is flat. The projection on the  $p$ -space of the submanifold  $p = f(x, u)$ , where  $x$  is considered as a parameter, is a ruled submanifold for all  $x$ .
- ▶ Otherwise stated: eliminating  $u$  from  $\dot{x} = f(x, u)$  yields a set of equations  $F(x, \dot{x}) = 0$ : for all  $(x, p)$  such that  $F(x, p) = 0$ , there exists  $a \in \mathbb{R}^n$ ,  $a \neq 0$  such that

$$\forall \lambda \in \mathbb{R}, \quad F(x, p + \lambda a) = 0.$$

- ▶ Proof elementary and derived from Hilbert (1912).
- ▶ Restricted version proposed by Sluis (1993).

Why static linearization coincides with flatness for single input systems ? Because a ruled-manifold of dimension 1 is just a straight line.

## Proving that a multi-input system is not flat

$$\frac{d}{dt}x_1 = u_1, \quad \frac{d}{dt}x_2 = u_2, \quad \frac{d}{dt}x_3 = (u_1)^2 + (u_2)^3$$

is not flat The submanifold  $p_3 = p_1^2 + p_2^3$  is not ruled: there is no  $a \in \mathbb{R}^3$ ,  $a \neq 0$ , such that

$$\forall \lambda \in \mathbb{R}, p_3 + \lambda a_3 = (p_1 + \lambda a_1)^2 + (p_2 + \lambda a_2)^3.$$

Indeed, the cubic term in  $\lambda$  implies  $a_2 = 0$ , the quadratic term  $a_1 = 0$  hence  $a_3 = 0$ .

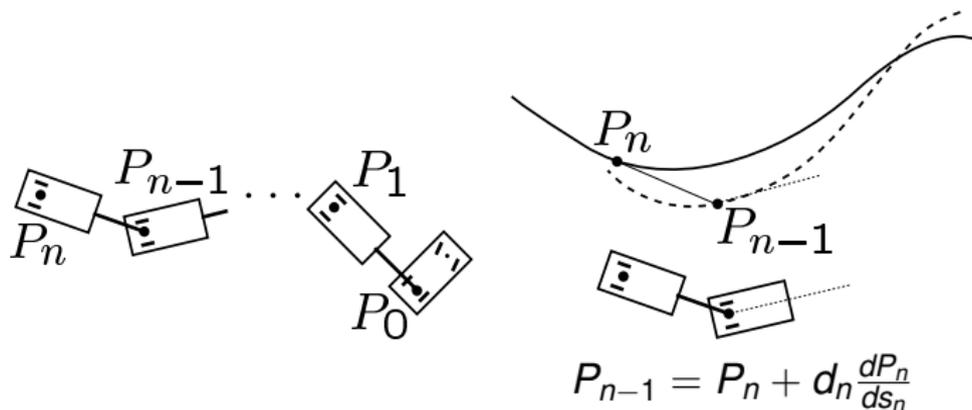
The system  $\frac{d}{dt}x_3 = \left(\frac{d}{dt}x_1\right)^2 + \left(\frac{d}{dt}x_2\right)^2$  does not define a ruled submanifold of  $\mathbb{R}^3$ : it is not flat in  $\mathbb{R}$ . But it defines a ruled submanifold in  $\mathbb{C}^3$ : in fact it is flat in  $\mathbb{C}$ , with the flat output

$$\begin{aligned} y_1 &= x_3 - (\dot{x}_1 - \dot{x}_2\sqrt{-1})(x_1 + x_2\sqrt{-1}) \\ y_2 &= x_1 + x_2\sqrt{-1}. \end{aligned}$$

## JBP result on equivalent systems SIAM JCO (2010)

- ▶ Take two explicit analytic systems  $\frac{d}{dt}x = f(x, u)$  and  $\frac{d}{dt}z = g(z, v)$  with  $\dim u = \dim v$  but not necessarily  $\dim x$  equals to  $\dim z$ . Assume that they are equivalent via a possible dynamic state feedback. Then we have
  - ▶ if  $\dim x < \dim z$  then  $\frac{d}{dt}x = f(x, u)$  is ruled.
  - ▶ if  $\dim z < \dim x$  then  $\frac{d}{dt}z = g(z, v)$  is ruled.
  - ▶ if  $\dim x = \dim z$  either they are equivalent by static feedback or they are both ruled.
- ▶ The system  $\frac{d}{dt}x = f(x, u)$  (resp.  $\frac{d}{dt}z = g(z, v)$ ) is said ruled when after elimination of  $u$  (resp.  $v$ ), the implicit system  $F(x, \frac{d}{dt}x) = 0$  (resp.  $G(z, \frac{d}{dt}z) = 0$ ) is ruled in the sense of the ruled manifold criterion explained here above.

## Geometric construction: $SE(2)$ invariance



- ▶ **Invariance** versus actions of the group  $SE(2)$ .
- ▶ Flat outputs are not unique:  $(\xi = x_n, \zeta = y_n + \frac{d}{dt}x_n)$  is **another flat output** since  $x_n = \xi$  and  $y_n = \zeta - \frac{d}{dt}\xi$ .
- ▶ The flat output  $(x_n, y_n)$  formed by the cartesian coordinates of  $P_n$  seems **more adapted** than  $(\xi, \zeta)$ : the output map  $h$  is **equivariant**.

Why the flat output  $z := (x, y)$  is better than the flat output  $\tilde{z} := (x, y + \dot{x})$  ?

Each symmetry of the system induces a transformation on the flat output  $z$

$$\begin{pmatrix} x \\ y \end{pmatrix} = \begin{pmatrix} z_1 \\ z_2 \end{pmatrix} \mapsto \begin{pmatrix} Z_1 \\ Z_2 \end{pmatrix} = \begin{pmatrix} X \\ Y \end{pmatrix} = \begin{pmatrix} z_1 \cos \alpha - z_2 \sin \alpha + a \\ z_1 \sin \alpha + z_2 \cos \alpha + b \end{pmatrix}$$

which does not involve derivatives of  $z$

This point transformation, generates an endogenous transformation  $(z, \dot{z}, \dots) \mapsto (Z, \dot{Z}, \dots)$  that is holonomic.

Why the flat output  $z := (x, y)$  is better than the flat output  $\tilde{z} := (x, y + \dot{x})$  ?

On the contrary

$$\begin{aligned} \begin{pmatrix} x \\ y + \dot{x} \end{pmatrix} = \begin{pmatrix} \tilde{z}_1 \\ \tilde{z}_2 \end{pmatrix} &\mapsto \begin{pmatrix} \dot{\tilde{z}}_1 \\ \dot{\tilde{z}}_2 \end{pmatrix} = \begin{pmatrix} X \\ Y + \dot{X} \end{pmatrix} \\ &= \begin{pmatrix} \tilde{z}_1 \cos \alpha + (\dot{\tilde{z}}_1 - \dot{\tilde{z}}_2) \sin \alpha + a \\ \tilde{z}_1 \sin \alpha + \tilde{z}_2 \cos \alpha + (\ddot{\tilde{z}}_1 - \ddot{\tilde{z}}_2) \sin \alpha + b \end{pmatrix} \end{aligned}$$

is not a point transformation and does not give to a holonomic transformation. It is endogenous since its inverse is

$$\begin{pmatrix} \dot{\tilde{z}}_1 \\ \dot{\tilde{z}}_2 \end{pmatrix} \mapsto \begin{pmatrix} \tilde{z}_1 \\ \tilde{z}_2 \end{pmatrix} = \begin{pmatrix} (\tilde{z}_1 - a) \cos \alpha - (\dot{\tilde{z}}_1 - \dot{\tilde{z}}_2) \sin \alpha \\ (\tilde{z}_1 - a) \sin \alpha + (\tilde{z}_2 - b) \cos \alpha - (\ddot{\tilde{z}}_1 - \ddot{\tilde{z}}_2) \sin \alpha \end{pmatrix}$$

## Symmetry preserving flat output

- ▶ Take the implicit system  $F(x, \dots, x^{(r)}) = 0$  with flat output  $y = h(x, \dots, x^{(\alpha)}) \in \mathbb{R}^m$  (i.e.  $x = \mathcal{A}(y, \dots, y^{(\beta)})$ )
- ▶ Assume that the **group  $G$  acting on the  $x$ -space** via the family of diffeomorphism  $X = \phi_g(x)$  ( $x = \phi_{g^{-1}}(X)$ ) leaves the ideal associated to the set of equation  $F = 0$  invariante:

$$F(x, \dots, x^{(r)}) = 0 \iff F\left(\phi_g(x), \dots, \phi_g^{(r)}(x, \dots, x^{(r)})\right) = 0$$

- ▶ **Question:** we wonder if exists always an **equivariante** flat output  $\bar{y} = \bar{h}(x, \dots, \bar{x}^{(\bar{\alpha})})$ , i.e. such that exists an action of  $G$  on the  $y$ -space via the family of diffeomorphisms  $\bar{Y} = \rho_g(\bar{y})$  satisfying

$$\rho_g(y) \equiv h\left(\phi_g(x), \dots, \phi_g^{(\bar{\alpha})}(x, \dots, x^{(\bar{r})})\right).$$

two different flat outputs correspond via a "**non-linear uni-modular transformation**":

$$\bar{y} = \psi(y, \dots, y^{(\mu)}) \quad \text{with inverse} \quad y = \bar{\psi}(\bar{y}, \dots, \bar{y}^{(\bar{\mu})})$$

## Flat outputs as potentials and gauge degree of freedom

Maxwell's equations in vacuum imply that the magnetic field  $H$  is divergent free:

$$\frac{\partial H_1}{\partial x_1} + \frac{\partial H_2}{\partial x_2} + \frac{\partial H_3}{\partial x_3} = 0$$

When  $H = \nabla \times A$  the constraint  $\nabla \cdot H = 0$  is automatically satisfied

The potential  $A$  is a priori not uniquely defined, but up to an arbitrary gradient field, the gauge degree of freedom. The symmetries indicate how to use this degree of freedom to fix a “natural” potential.

For flat systems: a flat output is a “potential” for the underdetermined differential equation  $\dot{x} - f(x, u) = 0$ ; endogenous transformations on the flat output correspond to gauge degrees of freedom.

## Open problems

- ▶  $\frac{d}{dt}x = f(x, u)$  with  $y = h(x, u, \dots, u^{(r)})$ ,  $r$ -flatness: bounds on  $r$  with respect to  $\dim(x)$  and  $\dim(u)$ .
- ▶ Symmetries and flat-output preserving symmetries: are time-invariant systems flat with a time invariant flat output map (a first step to prove that linearization via exogenous dynamics feedback, implies flatness).
- ▶ Are the intrinsic and extrinsic definitions of flat systems equivalent ?
- ▶ Flatness of JBP example

- ▶ The system

$$\frac{d}{dt}x_3 - x_2 - \left(\frac{d}{dt}x_1\right) \left(\frac{d}{dt}x_2 - x_3\frac{d}{dt}x_1\right)^2 = 0$$

is ruled with a single linear direction

$$a(x, \dot{x}) = (1, x_3, (\dot{x}_2 - x_3\dot{x}_1)^2)^T.$$

- ▶ There is no flat output  $y$  depending only on  $x$  and  $\dot{x}$  (this system is not 1-flat)
- ▶ **Conjecture:** this system is not flat.