

Prediction-based stabilization of linear systems subject to input-dependent input delay of integral-type

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Abstract—In this paper, it is proved that a predictor-based feedback controller can effectively yield asymptotic convergence for a class of linear systems subject to input-dependent input delay. This class is characterized by the delay being implicitly related to past values of the input via an integral model. This situation is representative of systems where transport phenomena take place, as is frequent in the process industry. The sufficient conditions obtained for asymptotic stabilization bring a local result and require the magnitude of the feedback gain to be consistent with the initial conditions scale. Arguments of proof for this novel result include general Halanay inequalities for delay differential equations and build on recent advances of backstepping techniques for uncertain or varying delay systems.

Index Terms—Time-delay systems, delay differential equation, prediction-based feedback, backstepping, partial differential equation

I. INTRODUCTION AND PROBLEM STATEMENT

Numerous control systems involve a physical lag which, as it is well known, reveals troublesome in the design and tuning of feedback control laws. In practice, such dead-time can occur when sensors and actuators are not co-located. Prime examples are processes involving transportation of material, such as mixing processes for liquid or gaseous fluids, chemical reactors [16], automotive engine [17] and exhaust line [13], heat collector plant [32], blending in liquid or solid networks [12], crushing mill [31] and batch processes [30], to name a few. Remarkably, in all these examples, the lag directly depends on the control variable and the considered delay is inherently input-dependent.

Surprisingly, it seems that stabilization of such processes with input-dependent delay in the input $D(u)$ or $D(u_t)$, where u_t denotes past values over a finite horizon, has seldom been theoretically studied. Rather, a widely considered approach is to neglect to various extents the control-dependency of the delay, e.g. by modeling this dependence as $D(u) \approx D(t)$ (or even by a constant average value D) and by asking the controller to deal with a certain level of unstructured delay uncertainty.

On the opposite, the methodology developed in this paper explicitly accounts for this dependency with the objective of

improving transient performances. The scope of this method is as follows: we investigate the following potentially unstable Single-Input Single-Output linear time-invariant plant¹, with a measured output $x(t)$,

$$x^{(n)} + a_{n-1}x^{(n-1)} + \dots + a_1\dot{x} + a_0x = b_0\varphi(t - D(t)) \quad (1)$$

driven by a delayed input, where the varying delay $D(t)$ is implicitly defined in terms of the input past values as

$$\int_{t-D(t)}^t \varphi(s)ds = 1 \quad \text{with} \quad \varphi(t) = \text{Sat}_{[\underline{u}, +\infty)}(u(t)), \quad \underline{u} > 0 \quad (2)$$

This system is depicted in Figure 1. The integral delay model² (2) corresponds to a Plug-Flow assumption [29] in a transport phenomenon and encompasses of a wide class of systems involving transport phenomena with velocity φ [7], [38]. It can be understood as the time of propagation for a transport process with time-varying speed for which the control variable is the speed itself³.

Motivating example An example of system fitting inside this framework is the one of the exhaust Fuel/Air Ratio (FAR) for Gasoline engines which can be found, e.g., in [7]. A schematic view of the system is pictured in Fig. 2. To optimize the catalyst operation, one wants to regulate the exhaust mixture composition λ to stoichiometry. This is done by injecting a given amount of fuel inside the combustion chamber, according to the current fresh air mass flow rate. However, such a variable fluctuates with the driver torque request (e.g., tip-ins and tip-outs). The main challenge while trying to improve the transient responses corresponding to these stimuli is that the injector (actuator) is located typically upstream of the combustion chamber. It is therefore spatially distant from the dynamics under consideration. This generates a transport delay (see [36]) which follows an integral relation of type (2).

In details, considering a given operating point (constant fresh air mass flow rate), defining $u(t)$ as the injected fuel

¹Potential existing zeros can still be handled by a suitable aforementioned choice of state-space representation and of the output matrix.

²Because $\varphi \geq \underline{u} > 0$, this transport delay is well-defined (positive and time-derivative bounded by one) and upper-bounded, $D(t) \leq \bar{D} \triangleq \frac{1}{\underline{u}}, t \geq 0$. Further, as $D \mapsto \int_{t-D}^t \varphi(s)ds$ is strictly increasing, it is invertible and the delay can be calculated. It is therefore considered as known in this paper.

³In details, it can be shown that the solution of the transport PDE $\partial_t \xi(x, t) = u(t) \partial_x \xi(x, t)$ for $x = [0, 1]$ satisfies $\xi(1, t) = \xi(0, t - D(t))$ with $D(t)$ defined by (2) (see [7]).

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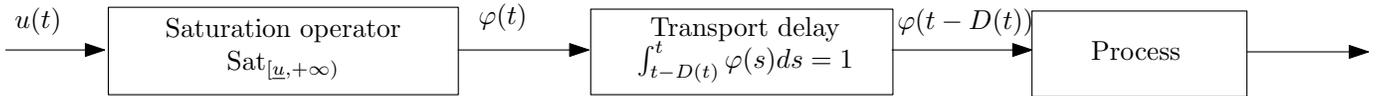


Fig. 1. The addressed problem, where the input is delayed by a transport delay which is input-varying.

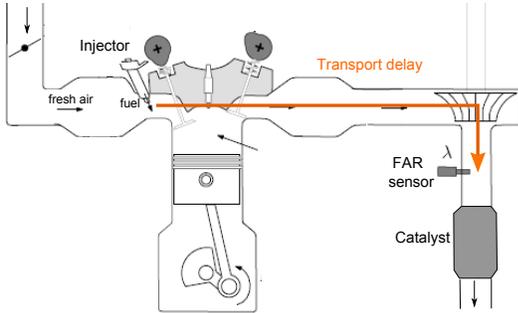


Fig. 2. Schematic view of the Fuel/Air Ratio system on a Gasoline engine equipped with indirect injection. A given amount of fuel is provided by the injector (actuator). The control objective here is to guarantee that the exhaust Fuel/Air Ratio, downstream of the catalyst (measured by an oxygen sensor), is close to stoichiometry.

flow rate and $x(t)$ as the exhaust FAR, which is the measured output, the dynamics can be written as a (stable) second-order input delay system (see [7] for specific modeling). The transport delay bearing on the input varies with the exhaust gas flow rate, which itself varies with the exhaust pressure [11]. The latter is a function of the injected fuel flow rate. Linearizing around the given operating point (potentially after normalization), one can recover an integral relation of type (2). Further, the input is lower-saturated to prevent the engine to stall (a minimum amount of fuel \underline{u} has to be injected for the mixture in the chamber to burn), which justifies the saturation in (2). Finally, we wish to stabilize the plant toward a positive equilibrium (stoichiometric exhaust composition) corresponding to a control reference $u^r > 0$.

Proposed methodology and comparison with state-of-the-art techniques The control objective at stake in this paper is to stabilize the plant (1)–(2) over any equilibrium point such that $x^r = \frac{b_0}{a_0} u^r$ with $u^r \geq \underline{u} > 0$. The reason why we only consider strictly positive steady-states is that, following (2), D tends to infinity while φ tends to zero. Therefore, in this case, the inputs do not reach the plant anymore and, obviously, unstable systems cannot be stabilized.

The solution we consider is a predictor-based control strategy (straightforwardly generalizing the ideas of [1], [24], [33]). Prediction is already widely used for systems with constant input time-delays (see for instance [8], [14], [19], [25], [26] or [31] and the references therein) but is still not of general use for time-varying delays (see [28] or, more recently, [22]). In such cases, to compensate the varying input delay, the prediction has to be calculated over a time window of which length matches the value of the future delay. In other words, one needs to predict the future variations of the delay to compensate it. For example, this is the approach followed

in [35] for a communication time-varying delay, the variations of which are provided by a given known model. It has also been used in [3], [4] for a state-dependent delay or in [5] for a delay depending on delayed state, where variations are anticipated by a careful prediction of the system state.

When the delay depends on the input, things are getting very involved. Determining the required prediction horizon becomes an implicit question, which may not be practically solvable nor even well-posed (this implicit interaction may yield to a set of conditions characterizing the time horizon which may be unsolvable for certain initial conditions). This implicit nature is caused by the reciprocal interactions between the control (current and past) values and the delay, yielding a closed-loop dependency.

For this reason, in this paper, in lieu of seeking exact delay compensation, we consider a prediction horizon equal to the current delay value. This does not prevent implicit mutual dependency between delay and input from arising, as the delay model (2) is input-varying and the delay is involved in the prediction-based control law. So, to disrupt this loop, which is particularly troublesome in the stability analysis, we use a two-steps methodology.

In a first move (Section II of this paper), we consider the input-dependency as a particular type of time-variations. This virtual parametrization suggests us to derive a robust compensation result for linear systems with time-varying input delay, using the backstepping tools proposed in [21] for the analysis of input-delay systems stability. Technically, this result guarantees stabilization provided that the delay variations are sufficiently small. This rather reasonable condition can be easily interpreted as a direct consequence of the approximation of the prediction interval by the current delay value. In a second step (Section III of this paper), to derive a more practical sufficient condition, the delay variations are related to the control tracking error fluctuations, which are analyzed using delay differential equations (DDE) stability theory (Halanay-type inequalities [15]). This methodology allows us to establish a result guaranteeing local exponential stability, i.e. Theorem 1, which yields exponential convergence of the system output towards x^r provided the initial conditions (x , its derivatives and the past values of the control $u_{[-D(0),0]}$) are sufficiently close to the equilibrium.

To the best of the authors' knowledge, this connection between prediction-based control law and input-dependency of the delay has not been studied earlier, except on preliminary works by the authors ([9] in which a scalar system is studied and [10] in which state-feedback is considered). The output prediction-based feedback proposed here for potentially unstable systems of order n subject the input-dependent delay (2), along with its proof of convergence in Theorem 1, is the main contribution of this paper.

The paper is organized as follows. In Section II, we address the topic of robust compensation of time-varying delay. Then, sufficient conditions for stabilization in the case of input-varying delay are derived in Section III through a proof of convergence invoking Halanay-like inequalities arguments. Finally, the merits of the obtained result are then illustrated in Section IV through simulations.

Notations and definitions

In the following, $|\cdot|$ stands for the usual Euclidean norm, $\|f(t)\|$ represents the norm of a spatially distributed variable $f : (x, t) \in [0, 1] \times \mathbb{R} \mapsto \mathbb{R}$ and is defined as

$$\|f(t)\| = \sqrt{\int_0^1 f(x, t)^2 dx} \quad (3)$$

$\mathcal{C}^0(S_1, S_2)$ (resp. $\mathcal{C}^1(S_1, S_2)$) denotes the set of continuous (resp. continuously differentiable) functions defined on a set S_1 with values into a set S_2 . The operator Sat_I stands for the standard saturation operator onto the interval I . For a given symmetric matrix, $\underline{\lambda}(\cdot)$ and $\bar{\lambda}(\cdot)$ stand respectively for minimum and maximum eigenvalues.

We write $\partial_x f$ the partial derivative of a function f with respect to a variable x . x_t refers to the function $x_t : s \in [-\bar{D}, 0] \mapsto x(t+s)$ for a given function x and a constant $\bar{D} > 0$. For any continuous function k defined on $[-\bar{D}, 0]$ and a polynomial function π , we write $\pi(x_t) = \pi\left(x(t_1), \dots, x(t_{n-2}), \int_{t_{n-1}}^{t_n} k(t-s)x(s)ds\right)$ for $(t_1, \dots, t_n) \in [t - \bar{D}, t]^n$.

A polynomial function π in the variables $(x_1, \dots, x_m, \dots, x_n)$ is said to be *at least quadratic* in x_1, \dots, x_m iff, for any given (x_{m+1}, \dots, x_n) , the corresponding polynomial function π_m defined as

$$\pi_m(x_1, \dots, x_m) = \pi(x_1, \dots, x_m, \dots, x_n) \quad (4)$$

has no terms of order 0 or 1, e.g. both $\pi = x_1^2 + x_1 x_2 x_3$ and $\pi = x_2 x_1 + x_3 x_1^2$ are at least quadratic in (x_1, x_2) while this is not the case for $\pi = x_3 + x_3 x_2^2$.

II. SUFFICIENT CONDITION FOR ROBUST COMPENSATION OF A TIME-VARYING INPUT DELAY

In this section, we consider the input delay as being any element of $\mathcal{C}^1(\mathbb{R}_+, [0, \bar{D}])$ for some \bar{D} . Here, to design our controller, we do not relate the variations of $D(t)$ to those of the control variable. To use the stabilization result established below, we first reformulate system (1)-(2) under a state-space representation

$$\begin{cases} \dot{X} = AX(t) + B\varphi(t - D(t)) \\ Y(t) = CX(t) \\ \int_{t-D(t)}^t \varphi(s)ds = 1 \quad \text{with} \quad \varphi(t) = \text{Sat}_{[\underline{u}, +\infty)}(u(t)) \end{cases} \quad (5)$$

where the pair (A, C) is observable and the controllable pair (A, B) is

$$A = \begin{pmatrix} 0 & 1 & & 0 \\ \vdots & & \ddots & \\ 0 & 0 & & 1 \\ -a_0 & -a_1 & \dots & -a_{n-1} \end{pmatrix}, \quad B = \begin{pmatrix} 0 \\ \vdots \\ 0 \\ b_0 \end{pmatrix} \quad (6)$$

Lemma 1: Consider the closed-loop single input system

$$\dot{X}(t) = AX(t) + Bu(t - D(t)) \quad (7a)$$

$$Y(t) = CX(t) \quad (7b)$$

$$\dot{\hat{X}}(t) = A\hat{X}(t) + Bu(t - D(t)) - L[Y(t) - C\hat{X}(t)] \quad (7c)$$

$$u(t) = K \left[e^{AD(t)} \hat{X}(t) + \int_{t-D(t)}^t e^{A(t-s)} Bu(s) ds \right] \quad (7d)$$

where $X \in \mathbb{R}^n$, $u \in \mathbb{R}$, K and L are chosen such that, respectively, $A + BK$ and $A + LC$ are Hurwitz and $D \in \mathcal{C}^1(\mathbb{R}_+, [0, \bar{D}])$ for some $\bar{D} > 0$. Define

$$\begin{aligned} \Upsilon_0(t) = & |X(t)|^2 + |X(t) - \hat{X}(t)|^2 + \int_{t-D(t)}^t u(s)^2 ds \\ & + D(t)^2 \int_{t-D(t)}^t \dot{u}(s)^2 ds \end{aligned} \quad (8)$$

There exists $\Delta^*(K) \in (0, 1)$ such that, if

$$\forall t \geq 0, \quad |\dot{D}(t)| < \Delta^*(K), \quad (9)$$

then there exist $R, \rho > 0$ such that

$$\forall t \geq 0, \quad \Upsilon_0(t) \leq R\Upsilon_0(0)e^{-\rho t} \quad (10)$$

and in particular the system state X of plant (7a) exponentially converges to the origin.

The prediction controller (7d) is a direct extension of the prediction over a constant delay time window to time-varying delay and output feedback, replacing respectively the constant delay by $D(t)$ and the system state by its observer \hat{X} . This controller aims at forecasting values of the state over a time window of varying length $D(t)$ ⁴. Of course, exact compensation of the delay is not achieved with this controller⁵ and can be highly inaccurate when the delay is fast varying. In this context, equation (9) can be interpreted as a condition for robust delay compensation achievement⁶. The spirit of this

⁴Note that, even if $\hat{X} = X$, this controller does not exactly match the predicted system state on a time-horizon $D(t)$. Indeed, using the variation of constant formula

$$\forall t \geq 0, \quad X(t + D(t)) = e^{AD(t)} X(t) + \int_{t-D(t)}^t e^{A(t-s)} Bu(s + D(t) - D(s)) ds$$

Under the assumption that the variations of the delay are sufficiently small, this latter integral can be approximated by the one used in (7d) as $D(t) - D(s) \approx 0$. As this assumption is already required to robustly compensate the delay, we rather use the prediction form (7d) which is easier to implement instead of the true prediction given above.

⁵As discussed earlier, to do so, one would need to consider a time window of which length would exactly match the value of the future delay, as it is made in [28] and [22]. In details, defining $\eta(t) = t - D(t)$ and assuming that its inverse exists (which is the case if $\dot{D} < 1$), exact delay-compensation is obtained with the feedback law $U(t) = KX(\eta^{-1}(t))$. Yet, implementing this relation requires to predict the future variation of the delay via $\eta^{-1}(t)$, which may not be practically achievable for an input-varying delay.

⁶Interestingly, a similar condition is often stated in Linear Matrix Inequality approaches, such as [37] for example, where the delay is also assumed to be time-differentiable.

condition is that, if the delay varies sufficiently slowly, its current value $D(t)$ used for prediction remains close enough to its future values, and the corresponding prediction is accurate enough to guarantee the stabilization of the plant through the feedback loop.

We now detail the proof of this result.

Proof In the following, we use the Lyapunov tools introduced in [21] to analyze the stability of input time-delay systems and which are based on a backstepping transformation of a certain actuator state defined for constant delays. First, we extend this distributed input to handle time-varying delay by defining $v(x,t) = u(t + D(t)(x-1))$, $x \in [0, 1]$ which enables to rewrite plant (7a)-(7c) as

$$\begin{cases} \dot{\tilde{X}}(t) &= (A+LC)\tilde{X}(t) \\ \dot{\hat{X}}(t) &= A\hat{X}(t) + Bv(0,t) - LC\tilde{X}(t) \\ D(t)\partial_t v(x,t) &= \partial_x v(x,t) + \dot{D}(t)(x-1)\partial_x v(x,t) \\ v(1,t) &= u(t) \end{cases} \quad (11)$$

in which the state observation error $\tilde{X} = X - \hat{X}$ has been introduced. In details, the input delay is now represented as a cascade with a transport partial differential equation (PDE) driven by the input and where the convection speed varies both with space and time. Pursuing the mentioned approach, now, consider the following backstepping transformation of the distributed input

$$w(x,t) = v(x,t) - D(t) \int_0^x K e^{AD(t)(x-y)} Bv(y,t) dy - K e^{AD(t)x} \hat{X}(t) \quad (12)$$

which is designed to satisfy $w(1,t) = 0$ compliantly with the choice of the control law (7d). The error equations (11) can now be rewritten as

$$\begin{cases} \dot{\tilde{X}}(t) &= (A+LC)\tilde{X}(t) \\ \dot{\hat{X}}(t) &= (A+BK)\hat{X}(t) + Bw(0,t) - LC\tilde{X}(t) \\ D(t)\partial_t w &= \partial_x w + \dot{D}(t)g(x,t) + DK e^{AD(t)x} LC\tilde{X}(t) \\ w(1,t) &= 0 \end{cases} \quad (13)$$

with

$$g(x,t) = (x-1)\partial_x v(x,t) - KD(t) \int_0^x e^{AD(t)(x-y)} Bv(y-1) \times \partial_x v(y,t) dy - KD(t) \left[\int_0^x e^{AD(t)(x-y)} (I + AD(t)(x-y)) \times Bv(y,t) dy + KAx e^{AD(t)x} \hat{X}(t) \right] \quad (14)$$

which can be formulated in terms of \tilde{X}, \hat{X}, w and w_x using the inverse Volterra equation corresponding to (12). For the Lyapunov analysis below, we also need the governing equation of the spatial derivative of this transformed distributed actuator which is

$$\begin{cases} D(t)\partial_{xt} w = \partial_{xx} w + \dot{D}(t)\partial_x g(x,t) + D^2 K e^{AD(t)x} ALC\tilde{X}(t) \\ \partial_x w(1,t) = -\dot{D}(t)g(1,t) - D(t)K e^{AD(t)} LC\tilde{X}(t) \end{cases} \quad (15)$$

We can now start the Lyapunov analysis and introduce the following Lyapunov-Krasovskii functional candidate

$$V(t) = \tilde{X}(t)^T P_0 \tilde{X}(t) + b_0 \hat{X}(t)^T P_1 \hat{X}(t) + b_1 D(t) \int_0^1 (1+x)[w(x,t)^2 + (\partial_x w(x,t))^2] dx \quad (16)$$

where P_0 and P_1 are the symmetric definite solutions of the two Lyapunov equations $(A+LC)^T P_0 + P_0(A+LC) = -Q_0$ and $(A+BK)^T P_1 + P_1(A+BK) = -Q_1$ for two given symmetric definite positive matrices Q_0 and Q_1 . Taking a time derivative of this functional and using integration by parts yield

$$\begin{aligned} \dot{V}(t) &= -\tilde{X}(t)^T Q_0 \tilde{X}(t) - b_0 \hat{X}(t)^T Q_1 \hat{X}(t) - b_1 w(0,t)^2 \\ &\quad + 2b_0 \hat{X}(t)^T P_1 Bw(0,t) - 2b_0 \hat{X}(t)^T P_1 LC\tilde{X}(t) - b_1 \|w(t)\|^2 \\ &\quad + 2b_1 (\partial_x w(1,t))^2 - b_1 (\partial_x w(0,t))^2 - b_1 \|\partial_x w(t)\|^2 \\ &\quad + 2b_1 \dot{D}(t) \int_0^1 (1+x)w(x,t)g(x,t) dx \\ &\quad + 2b_1 \int_0^1 (1+x)w(x,t)D(t)K e^{AD(t)x} LC\tilde{X}(t) dx \\ &\quad + 2b_1 \dot{D}(t) \int_0^1 (1+x)\partial_x w(x,t)\partial_x g(x,t) dx \\ &\quad + b_1 \dot{D}(t) \int_0^1 (1+x)[w(x,t)^2 + (\partial_x w(x,t))^2] dx \\ &\quad + 2b_1 \int_0^1 (1+x)\partial_x w(x,t)D(t)^2 K e^{AD(t)x} ALC\tilde{X}(t) dx \end{aligned} \quad (17)$$

To bound the remaining terms, one can introduce the inverse transformation of (12)

$$v(x,t) = w(x,t) + D(t)K \int_0^x e^{(A+BK)D(t)(x-y)} Bw(y,t) dy + K e^{(A+BK)D(t)x} \hat{X}(t) \quad (18)$$

and its spatial derivative to obtain, using Cauchy-Schwartz's and Young's inequality, the existence of positive constants M_1, M_2, M_3 and M_4 such that

$$\begin{aligned} &\left| 2 \int_0^1 (1+x)w(x,t)g(x,t) dx \right| \\ &\leq M_1 \left(|\hat{X}(t)|^2 + \|w(t)\|^2 + \|w_x(t)\|^2 \right) \end{aligned} \quad (19)$$

$$\begin{aligned} &\left| 2 \int_0^1 (1+x)w(x,t)D(t)K e^{AD(t)x} LC\tilde{X}(t) dx \right| \\ &\leq M_2 |\tilde{X}(t)|^2 + \frac{\|w(t)\|^2}{2} \end{aligned} \quad (20)$$

$$\begin{aligned} &\left| 2 \int_0^1 (1+x)\partial_x w(x,t)\partial_x g(x,t) dx \right| \\ &\leq M_3 \left(|\hat{X}(t)|^2 + \|w(t)\|^2 + \|\partial_x w(t)\|^2 + (\partial_x w(0,t))^2 \right) \end{aligned} \quad (21)$$

$$\begin{aligned} &\left| 2 \int_0^1 (1+x)\partial_x w(x,t)D(t)^2 K e^{AD(t)x} ALC\tilde{X}(t) dx \right| \\ &\leq M_4 |\tilde{X}(t)|^2 + \frac{\|\partial_x w(t)\|^2}{2} \end{aligned} \quad (22)$$

$$\begin{aligned} 2(\partial_x w(1,t))^2 &\leq M_6 |\tilde{X}(t)|^2 \\ &\quad + M_5 |\dot{D}(t)|^2 \left(|\hat{X}(t)|^2 + \|w(t)\|^2 + \|\partial_x w(t)\|^2 \right) \end{aligned} \quad (23)$$

Further, using Young's inequality, we have that

$$|2b_0\hat{X}(t)^T P_1 B w(0,t)| \leq \frac{b_0\lambda(Q_1)}{4} |\hat{X}(t)|^2 + \frac{4b_0}{\lambda(Q_1)} |P_1 B|^2 w(0,t)^2 \quad (24)$$

$$|2b_0\hat{X}(t)^T P_1 LC \tilde{X}(t)| \leq \frac{b_0\lambda(Q_1)}{4} |\hat{X}(t)|^2 + \frac{4b_0}{\lambda(Q_1)} |P_1 LC|^2 |\tilde{X}(t)|^2 \quad (25)$$

Therefore, defining the intermediate functional $V_0 = |\tilde{X}(t)|^2 + |\hat{X}(t)|^2 + \|w(t)\|^2 + \|\partial_x w(t)\|^2$, using (19)–(25) and regrouping terms, it is straightforward to get

$$\begin{aligned} \dot{V}(t) \leq & -\frac{b_0\lambda(Q_1)}{2} |\hat{X}(t)|^2 - \left(b_1 - 4\frac{b_0}{\lambda(Q_1)} |P_1 B|^2 \right) w(0,t)^2 \\ & - \left(\lambda(Q_0) - 4\frac{b_0}{\lambda(Q_1)} |P_1 LC|^2 - b_1(M_2 + M_6 + M_4) \right) |\tilde{X}(t)|^2 \\ & - \frac{b_1}{2} \|w(t)\|^2 - \frac{b_1}{2} \|\partial_x w(t)\|^2 - b_1(1 - |\dot{D}(t)|M_3) (\partial_x w(0,t))^2 \\ & + |\dot{D}(t)| b_1 (M_1 + M_5 |\dot{D}(t)| + M_3 + 2) V_0 \end{aligned} \quad (26)$$

Consequently, by choosing $b_1 = \frac{8b_0}{\lambda(Q_1)} |P_1 B|^2$ and $b_0 = \frac{\lambda(Q_0)\lambda(Q_1)}{8(|P_1 LC|^2 + 2(M_2 + M_4 + M_6)|P_1 B|^2)}$, one can define

$$\eta = \min \left\{ \frac{\lambda(Q_0)}{2}, \frac{b_0\lambda(Q_1)}{2}, \frac{b_1}{2} \right\} \quad (27)$$

$$\Delta^*(K) = \min \left\{ 1, \frac{1}{M_3}, \frac{\eta}{b_1(M_1 + M_5 + M_3 + 2)} \right\} \quad (28)$$

and obtain that, if $|\dot{D}(t)| < \Delta^*(K)$, $t \geq 0$, then there exists $\mu > 0$ such that

$$\begin{aligned} \dot{V}(t) & \leq -\mu V_0(t) \\ & \leq -\frac{\mu}{\max \{ \bar{\lambda}(P_0), b_0 \bar{\lambda}(P_1), 2b_1 \bar{D} \}} V(t) = -\mu_1 V(t) \end{aligned} \quad (29)$$

in which μ_1 is a positive constant. Consequently,

$$\forall t \geq 0, \quad V(t) \leq V(0)e^{-\mu_1 t} \quad (30)$$

Finally, one can reformulate this result in terms of the functional Y_0 . Indeed, using a simple change of variable, Y_0 can be rewritten as

$$Y_0(t) = |X(t)|^2 + |\tilde{X}(t)|^2 + D(t) \|v(t)\|^2 + D(t) \|\partial_x v(t)\|^2 \quad (31)$$

Then, using (18) together with Young's inequality, one can establish the following inequalities

$$\|v(t)\|^2 \leq r_1 |\hat{X}(t)|^2 + r_2 \|w(t)\|^2 \quad (32)$$

$$\|\partial_x v(t)\|^2 \leq r_3 |\hat{X}(t)|^2 + r_4 \|w(t)\|^2 + r_5 \|\partial_x w(t)\|^2 \quad (33)$$

$$\|w(t)\|^2 \leq s_1 |\hat{X}(t)|^2 + s_2 \|v(t)\|^2 \quad (34)$$

$$\|\partial_x w(t)\|^2 \leq s_3 |\hat{X}(t)|^2 + s_4 \|v(t)\|^2 + s_5 \|\partial_x v(t)\|^2 \quad (35)$$

where $r_1, r_2, r_3, r_4, r_5, s_1, s_2, s_3, s_4$ and s_5 are positive constants. Therefore, using (32)–(35), one can obtain, for $t \geq 0$,

$$\begin{aligned} & \frac{1}{\max \{ \bar{\lambda}(P_0) + b_0 \bar{\lambda}(P_1), 2b_1 \}} V(t) \\ & \leq Y_0(t) \leq \frac{\max \{ 3, 2 + \bar{D}r_1 + \bar{D}r_3, r_2 + r_4, r_5 \}}{\min \{ \lambda(P_0), b_0 \lambda(P_1), b_1 \}} V(t) \end{aligned} \quad (36)$$

The existence of two positive constants ρ and R such that (10) holds directly follows. This concludes the proof of the Lemma. \blacksquare

III. CONTROL DESIGN

In this section, we now establish a sufficient condition guaranteeing (9) when the delay varies according to the integral relation (2). This new condition bears on the initial conditions (accordingly to the choice of the control gain).

Theorem 1: Consider the closed-loop system

$$\dot{X}(t) = AX(t) + B\varphi(t - D(t)) \quad (37)$$

$$Y(t) = CX(t) \quad (38)$$

$$\dot{\hat{X}}(t) = A\hat{X}(t) + B\varphi(t - D(t)) - L(Y(t) - C\hat{X}(t)) \quad (39)$$

$$\int_{t-D(t)}^t \varphi(s) ds = 1 \quad \text{with} \quad \varphi(t) = \text{Sat}_{[\underline{u}, +\infty)}(u(t)) \quad (40)$$

$$u(t) = u^r + K \left[e^{AD(t)} \hat{X}(t) + \int_{t-D(t)}^t e^{A(t-s)} B\varphi(s) ds - X^r \right] \quad (41)$$

where A and B are defined in (6), K is such that $A + BK$ is Hurwitz, L is such that $A + LC$ is Hurwitz and with distinct eigenvalues, X^r is the state equilibrium corresponding to the original equilibrium x^r of plant (1) and u^r is the corresponding (constant) control reference. Consider the functionals

$$\Theta(t) = |X(t) - \hat{X}(t)| + \max_{s \in [t-\bar{D}, t]} \left| \left[u(s) - u^r \quad \dot{u}(s) \dots u^{(n-1)}(s) \right]^T \right| \quad (42)$$

$$\begin{aligned} \Upsilon(t) & = |X(t) - X^r|^2 + |X(t) - \hat{X}(t)|^2 + \int_{t-D(t)}^t (u(s) - u^r)^2 ds \\ & \quad + D(t)^2 \int_{t-D(t)}^t \dot{u}(s)^2 ds \end{aligned} \quad (43)$$

Then, provided that $u_0 \in \mathcal{C}^n([-D, 0], \mathbb{R})$, there exists $\theta: \mathbb{R}^n \mapsto \mathbb{R}_+^*$ such that if $\Theta(0) < \theta(K)$ condition (9) is fulfilled and the plant exponentially converges in the sense that there exist $R, \rho > 0$ such that

$$\forall t \geq 0, \quad \Upsilon(t) \leq RY(0)e^{-\rho t} \quad (44)$$

This result has a relatively direct interpretation: the previously presented Lemma 1 requires the delay to vary sufficiently slowly, while, on the other hand, here the delay variations implicitly depend on the control input through the integral equation (2), with variations which aggressiveness is scaled by the gain K . Then, restricting the input variations by choosing the initial conditions close enough to the desired equilibrium and in compliance with the feedback gain magnitude seems like a natural requirement.

The behavior of the function θ with respect to its argument K could be investigated in future works but is not pursued here. A constructive expression of this function is given through (27), (84) and (90). From this expression, the study would involve to analyze the solution of the Lyapunov equation and the behavior of its eigenvalues with respect to K variations. One could reasonably assume that $\theta(K) \rightarrow 0$ while $K \rightarrow -\infty$ (as $r(K)$ is expected in this case to tend to ∞). Therefore, for given initial conditions, the magnitude of the feedback

gain should be chosen accordingly. For relatively large initial conditions, this would imply to use a small feedback gain, as illustrated below in Section IV. Therefore, this result can be interpreted as a small-gain condition.

Also, one can note that the requirement $u_0 \in \mathcal{C}^n([-D, 0], \mathbb{R})$ implies that the control is continuous at $t = 0$, that is $u_{[-D, 0]}$ is consistent with the value $u(0)$ imposed by the prediction-based control law (41). Such a condition can seem demanding from an application point of view, but, as emphasized in the illustration section, is not necessary in practice. Future developments will focus on the extension of this result to handle discontinuities at $t = 0$.

Finally, we wish to compare our result to robustness approaches proposed, e.g. in [6], [20]. At first glance, it could seem that Lemma 1 in which the proposed result is built on is somehow restrictive in the sense that it requires the delay rate to be sufficiently small. In the two provided references, a nominal value of the delay is used and stabilization is guaranteed provided less demanding assumption on the delay disturbances. However, we would like to emphasize two points. First, for the considered integral relation (2), recasting the input-dependency as a delay perturbation does not seem like a natural move. Second, even if one decides to pick the nominal value $D^r = 1/u^r$, one cannot a priori check that the delay disturbance $\delta(t) = D(t) - D^r$ will satisfy the conditions of [6]. The same holds for the requirement on the size of the delay perturbation established in [20] which may not be fulfilled. Guaranteeing that one of these conditions holds for $D(t) - D^r$ requires a deeper analysis such as the one proposed in the sequel. Finally, by using the exact current delay value $D(t)$ in the prediction in lieu of a nominal one (D^r for instance), we aim at improving delay compensation and therefore transient performance. We illustrate this point in simulations in Section IV.

We now detail the proof of Theorem 1.

A. Relating the delay variations to input variations

Taking a time-derivative of (40) and defining the error variable

$$\varepsilon \triangleq \varphi - u^r \quad (45)$$

one gets, using $\varphi \geq \underline{u}$,

$$|\dot{D}(t)| = \left| 1 - \frac{\varepsilon(t) + u^r}{\varepsilon(t - D(t)) + u^r} \right| \leq \frac{2 \max |\varepsilon_t|}{\underline{u}} \quad (46)$$

As a result, condition (9) is satisfied if

$$\forall t \geq 0, \quad \max |\varepsilon_t| < \frac{\underline{u} \Delta^*(K)}{2} \quad (47)$$

This is the condition we now focus on. It yields to the analysis of the dynamics of the variable ε . Before properly starting this analysis, we recall and extend some well-known stability results for DDE.

B. Preliminary results : extension of the Halanay inequality for Delay Differential Equations of order $n \geq 1$

We first recall the following result [15], [18]⁷ which was generalized in recent works [23], [34].

Lemma 2 (Halanay inequality): Consider a positive continuous real-valued function x such that

$$\dot{x}(t) \leq -ax(t) + b \max x_t, \quad t \geq 0 \quad (48)$$

with $a \geq b \geq 0$. Then, there exists $\gamma \geq 0$ such that

$$\forall t \geq 0, \quad x(t) \leq \max x_0 e^{-\gamma t} \quad (49)$$

A straightforward extension of this lemma is stated in the corollary below.

Corollary 1: Consider a positive continuous function such that

$$\begin{cases} \dot{x}(t) & \leq -ax(t) + bh(t) + ce^{-\gamma t}, \quad t \geq 0 \\ x_0 & = \psi \in \mathcal{C}^0([-D, 0], \mathbb{R}_+) \end{cases} \quad (50)$$

where $a \geq b \geq 0$, $\gamma > 0$ and h is a continuous functional satisfying, for some $\omega > 0$, the sup-norm relation

$$|h(t)| \leq \max |x_t|, \quad \text{for } \max |x_t| < \omega \quad (51)$$

Then, if the initial condition is such that $\max \psi < \omega$, there exists $c_\omega^* > 0$ (depending on ω) such that, if $|c| < c_\omega^*$, then there exists $\tilde{\gamma} \in [0, \gamma)$ ($\tilde{\gamma} = 0$ if $a = b$ and $\tilde{\gamma} > 0$ otherwise) such that

$$\forall t \geq 0, \quad x(t) \leq \max \{ \max x_0, \mu^*(|c|, \gamma, \gamma_0) \} e^{-\tilde{\gamma} t} \quad (52)$$

in which μ^* is defined in terms of γ_0 , the unique non-negative solution of the equation $\gamma_0 - a + be^{\gamma_0 D} = 0$, as

$$\mu^*(|c|, \gamma, \gamma_0) = \begin{cases} 0 & \text{if } \gamma_0 = 0 \\ \max \left\{ \frac{1}{a - be^{\gamma_0 D} - \gamma}, \frac{1 - \frac{\gamma}{\gamma_0}}{a - be^{\gamma_0 D} - \gamma} \right\} \geq 0 & \text{if } \gamma \neq \gamma_0 \\ \frac{1}{\gamma(1 + bDe^{\gamma_0 D})} & \text{otherwise} \end{cases} \quad (53)$$

In the particular case $\omega = +\infty$, one can notice from the elements of proof detailed below that $c_\omega^* = +\infty$, i.e. this result holds for any value of $c \in \mathbb{R}$, thanks to the global inequality (51).

Proof Consider x a non-trivial positive and continuous solution⁸ of (50), with $\max \psi < \omega$. On a certain neighborhood (at least) of the origin $t = 0$, from (51) and by continuity, it satisfies the inequality

$$\dot{x}(t) \leq -ax(t) + b \max x_t + |c|e^{-\gamma t} \quad (54)$$

Following the spirit of the original proof in [15], we first consider a positive solution of the corresponding differential equation

$$\dot{y}(t) = -ay(t) + b \max y_t + |c|e^{-\gamma t}, \quad t \geq 0 \quad (55)$$

⁷More precisely, in [15], this result is stated for $a > b > 0$.

⁸The existence of such a continuous function is obtained by considering the equality corresponding to (50) for which continuous (and even more) solutions exist assuming the initial condition ψ smooth enough [2]. Such a solution is then also a solution of the inequality (50).

with a given initial condition such that $y(0) = \mu > 0$, where the constant μ will be chosen adequately below. Defining γ_0 as the unique non-negative solution of the equation $\gamma_0 - a + be^{\gamma_0 \bar{D}} = 0$, some computations show that a suitable function y is

$$\forall t \in \mathbb{R}, y(t) = \begin{cases} \frac{|c|}{a - be^{\gamma \bar{D}} - \gamma} e^{-\gamma t} + \left(\mu - \frac{|c|}{a - be^{\gamma \bar{D}} - \gamma} \right) e^{-\gamma_0 t} & \text{if } \gamma \neq \gamma_0 \\ \left(\frac{|c|}{1 + b\bar{D}e^{\gamma \bar{D}}} t + \mu \right) e^{-\gamma t} & \text{otherwise} \end{cases} \quad (56)$$

which is positive and decreasing by choosing (if $\gamma_0 > 0$) $\mu > \mu^*(|c|, \gamma, \gamma_0)$ where μ^* is defined in (53)⁹. One can also show that there exists $\tilde{\gamma} \in [0, \min\{\gamma, \gamma_0\})$ such that

$$\forall t \geq 0, y(t) \leq \mu e^{-\tilde{\gamma} t} \quad (57)$$

Indeed, (i) when $\gamma_0 \neq \gamma$, this directly follows from the expression (56) and (ii) when $\gamma_0 = \gamma$, $\tilde{\gamma} \geq 0$ exists as $\mu > \mu^*(|c|, \gamma)$. In details, if $\gamma_0 > 0$ (i.e. $a > b$), there exists $\tilde{\gamma} > 0$ and $\tilde{\gamma} = 0$ otherwise.

Now, define the difference $z = y - x$ which is a continuous function. We aim at choosing the initial condition of y such that $z(t) > 0$ for $t \in [-\bar{D}, 0]$, i.e. $\mu > \max x_0$. Further, to take advantage of (51), we would like to guarantee that $\max y(t) < \omega$ for all $t \geq 0$. Gathering all these conditions, this finally implies to choose $\mu \in (0, \omega) \cap (\max\{\max x_0, \mu^*(c)\}, \infty)$. Provided $\mu^*(|c|) < \omega$, this set is non-empty as $\max x_0 < \omega$. Let us now discuss this assumption. For given parameters a, b and γ , μ^* is a linear function of $|c|$. Therefore, there exists $c_\omega^* > 0$ such that, for $|c| < c_\omega^*$, $\mu^*(|c|) < \omega$ and the choice of μ is valid.

We are now interested in the (potential) sign change of z . As the function z is continuous, we consider

$$t_1 = \inf\{t > 0 | z(t) = 0\} \in \mathbb{R} \quad (58)$$

Assume that t_1 is well-defined. From its definition, $z(t) > 0$ for $t \in [0, t_1)$ and, from the analytical expression of y and as both x and y are continuous, $x(t) < y(t) \leq \mu < \omega$ for $t \in [0, t_1)$. Hence, the following inequality holds

$$\forall t \in [0, t_1), \quad \dot{z}(t) + az(t) \geq b(\max y_t - \max x_t) \quad (59)$$

Then, $\dot{z}(t_1) \geq \max y_{t_1} - \max x_{t_1} > 0$, by definition of t_1 . Yet, one has

$$\dot{z}(t_1) = \lim_{t \rightarrow t_1^-} \frac{z(t) - z(t_1)}{t - t_1} = \lim_{t \rightarrow t_1^-} \frac{z(t)}{t - t_1} \leq 0 \quad (60)$$

as $z(t) \geq 0$ on $[0, t_1]$. This contradiction allows us to conclude that such an instant t_1 does not exist and that, $\forall t \geq 0, z(t) > 0$. Finally, using (57),

$$\forall t \geq 0 \quad x(t) \leq \max\{\max x_0, \mu^*(|c|, \gamma, \gamma_0)\} e^{-\tilde{\gamma} t} \quad (61)$$

which is the desired result. \blacksquare

⁹ μ^* is always positive for $\gamma_0 > 0$. Indeed, if $\gamma \neq \gamma_0$, the second coefficient involved in its definition through the max function is strictly positive. Specifically, for $\gamma < \gamma_0$, $a - be^{\gamma \bar{D}} - \gamma > 0$ and $1 - \gamma/\gamma_0 > 0$ and, for $\gamma > \gamma_0$, $a - be^{\gamma \bar{D}} - \gamma < 0$ and $1 - \gamma/\gamma_0 < 0$

Lemma 3 (stability of a n^{th} order DDE): Let x be a solution of the n^{th} order DDE

$$\begin{cases} x^{(n)} + \alpha_{n-1}x^{(n-1)} + \dots + \alpha_0x = \\ \beta_1 \ell_1(t, x_t, \dots, x_t^{(n-1)}) + \beta_2 \ell_2(t), & \text{for } t \geq 0 \\ [x \dots x^{(n-1)}]_0^T = \psi \in \mathcal{C}^0([-\bar{D}, 0], \mathbb{R}^n) & \text{with } \max |\psi| < \omega \end{cases} \quad (62)$$

where the left-hand side of the differential equation defines a polynomial function the roots of which have strictly negative real part, $\omega > 0$, $\beta_1 \geq 0$, β_2 is a scalar constant and ℓ_1 and ℓ_2 are continuous functionals. There exist $\beta_{\max}^1 > 0$, $\beta_{\max}^2 > 0$ and $r_* > 0$ ($\beta_{\max}^1 = \alpha_0$, $\beta_{\max}^2 = \infty$ and $r_* = 1$ if $n = 1$) such that, if

- 1) $0 \leq \beta_1 < \beta_{\max}^1$ and $|\beta_2| < \beta_{\max}^2$;
- 2) there exists $\gamma > 0$ such that $|\ell_2(t)| \leq e^{-\gamma t}$ for $t \geq 0$;
- 3) ℓ_1 satisfies the following sup-norm relation, with $X \triangleq [x \ \dot{x} \dots x^{(n-1)}]^T$,

$$\forall t \geq t_0, \quad |\ell_1(t, x_t, \dots, x_t^{(n-1)})| \leq \max |X_t| \quad (63)$$

for $t \geq 0$, $\max |X_t| < r\omega$ with $r \geq r_*$

then, there exists $\tilde{\gamma} \in (0, \gamma)$ and $R > 0$ such that

$$\forall t \geq 0, \quad |X(t)| \leq \max\{r_* \max |X_0|, R\beta_2\} e^{-\tilde{\gamma} t} \quad (64)$$

Proof The idea is to use the scalar result of Corollary 1. Define the scalar-valued function $m(t) \triangleq X(t)^T P X(t)$ where P is, as defined in the statement of the Lemma, the symmetric positive definite matrix solution of the Lyapunov equation $A_0^T P + P A_0 = -Q$, for some given symmetric positive definite matrix Q , and A_0 is the companion matrix

$$A_0 = \begin{pmatrix} 0 & 1 & & & \\ \vdots & & \ddots & & \\ 0 & & & & 1 \\ -\alpha_0 & -\alpha_1 & \dots & -\alpha_{n-1} & \end{pmatrix} \quad (65)$$

Define $a \triangleq \frac{\underline{\lambda}(Q)}{2\bar{\lambda}(P)}$, $b \triangleq 2\beta_1 \frac{\bar{\lambda}(P)}{\bar{\lambda}(P)}$ and $c = \frac{2\beta_2 \bar{\lambda}(P)^2}{\bar{\lambda}(Q)}$. Taking a time-derivative of m and, classically, applying Young's inequality, one can obtain

$$\dot{m}(t) \leq -am(t) + bh(t) + ce^{-2\tilde{\gamma} t} \quad (66)$$

with

$$\begin{aligned} h(t) &= \frac{\underline{\lambda}(P)}{\beta_1 \bar{\lambda}(P)} X(t)^T P \begin{pmatrix} 0 \\ \vdots \\ 0 \\ \beta_1 \ell_1(\cdot) \end{pmatrix} \\ &\leq \sqrt{\underline{\lambda}(P)} \sqrt{m(t)} |\ell_1(t, x_t, \dots, x_t^{(n-1)})| \end{aligned} \quad (67)$$

which satisfies, for $\max |X_t| < r\omega$ (and therefore, in particular, for $\max m_t < r^2 \omega^2 \underline{\lambda}(P)$),

$$|h(t)| \leq \sqrt{m(t)} \max \sqrt{m_t} \leq \max m_t \quad (68)$$

Define the condition

$$\max m_0 < r^2 \omega^2 \underline{\lambda}(P) \quad (69)$$

If (69) holds, then one concludes, applying Corollary 1, that there exists $c_\omega^* > 0$ such that, if $|c| < c_\omega^*$ and $a > b$, then there exists $\tilde{\gamma} \in (0, \gamma)$ such that

$$\forall t \geq 0, \quad m(t) \leq \max \{ \max |m_{t_0}|, \mu^* \} e^{-2\tilde{\gamma}t} \quad (70)$$

in which μ^* is defined in (53). Yet, a sufficient condition for $\max m_0 < r^2 \omega^2 \underline{\lambda}(P)$ to hold is that $\max |X_0|^2 < r^2 \omega^2 \frac{\underline{\lambda}(P)}{\underline{\lambda}(P)}$. By assumption, $\max |X_0| < \omega$. Hence, to guarantee that (69) holds, one simply has to pick $r \geq r_* \triangleq \sqrt{\frac{\underline{\lambda}(P)}{\underline{\lambda}(P)}}$. Finally, the condition $a > b$ can be reformulated as $\beta_1 < \frac{\underline{\lambda}(P)\underline{\lambda}(Q)}{4\underline{\lambda}(P)^2} \triangleq \beta_{\max}^1$, the condition $|c| < c_\omega^*$ as $|\beta_2| < \sqrt{\frac{c_\omega^*\underline{\lambda}(Q)}{2\underline{\lambda}(P)^2}} \triangleq \beta_{\max}^2$ and one obtains

$$\forall t \geq t_0, \quad |X(t)| \leq \max \left\{ \sqrt{\frac{\underline{\lambda}(P)}{\underline{\lambda}(P)}} \max |X_0|, \sqrt{\frac{\mu^*}{\underline{\lambda}(P)}} \right\} e^{-\tilde{\gamma}t} \quad (71)$$

which concludes the proof. \blacksquare

C. Proof of Theorem 1 - Application of Halanay-like inequality to dynamical equation of the input error variable ε

To obtain a sufficient condition guaranteeing (47), we first focus on the DDE governing ε , which is given in the following lemma.

Lemma 4: Consider $t_0 \in \mathbb{R}$ and assume that the function φ is unsaturated for $t \leq t_0$ (or equivalently that $u(t) \geq \underline{u}$, $t \leq t_0$). Provided that $u_0 \in \mathcal{C}^n([-D, 0], \mathbb{R})$, the error variable $\varepsilon = u - u^r$ with u defined in (41) is n times continuously differentiable for $t \geq t_0$ and satisfies the following differential equation for $t \geq t_0$

$$\begin{aligned} & \varepsilon^{(n)} + (a_{n-1} + b_0 k_{n-1}) \varepsilon^{(n-1)} + \dots + (a_0 + b_0 k_0) \varepsilon \\ &= \pi_1 \left(\dot{D}, \dots, D^{(n)}, \varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \tilde{X}, \frac{1}{1+D} \right) \\ &+ K \pi_2 \left(\dot{D}, \dots, D^{(n)} \right) \tilde{X}(t) \end{aligned} \quad (72)$$

where the constants k_i ($i \in \{1, \dots, n-1\}$) are such that $[-k_0 \dots -k_{n-1}] \triangleq K$, π_1 and π_2 are polynomial functions and π_1 is *at least quadratic* in the variables $\dot{D}, \dots, D^{(n)}, \varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \tilde{X}$.

Proof For sake of clarity, the proof of this theorem is given in Appendix. \blacksquare

Now that we are equipped with this last lemma, it is possible to use Lemma 3 to guarantee that the stability condition (47) holds.

Lemma 5: Consider the functional Θ defined in (42). Provided that $u_0 \in \mathcal{C}^n([-D, 0], \mathbb{R})$, there exists $\theta : \mathbb{R}^n \mapsto \mathbb{R}_+^*$ such that, if $\Theta(0) < \theta(K)$, then

$$\forall t \geq 0, \quad |\varepsilon(t)| \leq \min \left\{ \frac{u \Delta^*(K)}{2}, u^r - u \right\} \quad (73)$$

which implies that condition (47) is fulfilled.

Proof Assume for a moment that the function φ is not saturated for $t \leq 0$. Then, dynamics (72) holds and is compliant with the assumptions of Lemma 3.

In details, first, the left-hand side of (72) is asymptotically stable, as it represents the last line of the Hurwitz companion matrix $A + BK$. Second, by observing that

$$\dot{D} = \frac{\varepsilon(t-D) - \varepsilon(t)}{\varepsilon(t-D) + u^r} \quad (74)$$

one can obtain by induction that, for $m \geq 1$, $D^{(m)}$ is a polynomial function in $\varepsilon_t, \dots, \varepsilon_t^{(m-1)}, \frac{1}{\varepsilon(t-D) + u^r}$ without any term of order 0 or 1. Therefore, π_1 is directly a polynomial function of the variables $\varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \tilde{X}, \frac{1}{1+D}, \frac{1}{\varepsilon(t-D) + u^r}$, which is *at least quadratic* in the variables $\varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \tilde{X}$ and π_2 is a polynomial function in $\varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \frac{1}{\varepsilon(t-D) + u^r}$.

Now, we distinguish some of the terms in π_1 and π_2 . First, consider $c_{2,0}$ the constant term of π_2 and $c_{2,1}$ the term of first order in π_2 involving $\frac{1}{\varepsilon(t-D) + u^r}$. Further, consider $c_{1,2}$ the terms in π_1 involving \tilde{X} at power 1 and only one of the variables $\varepsilon_t, \dots, \varepsilon_t^{(n-1)}$ and at power 1. This term can be written as follows

$$c_{1,2} = \pi_3 \left(\varepsilon_t, \dots, \varepsilon_t^{n-1}, \frac{1}{1+D}, \frac{1}{\varepsilon(t-D) + u^r} \right) \tilde{X} \quad (75)$$

in which π_3 is a (vectorial) polynomial function the terms of which involve exactly one of the variables $\varepsilon_t, \dots, \varepsilon_t^{n-1}$. Now, applying Young's inequality, one can obtain

$$|c_{1,2}| \leq \frac{1}{2} \left| \pi_3 \left(\varepsilon_t, \dots, \varepsilon_t^{n-1}, \frac{1}{1+D}, \frac{1}{\varepsilon(t-D) + u^r} \right) \right|^2 + \frac{|\tilde{X}(t)|^2}{2} \quad (76)$$

in which $|\pi_3|^2$ is now a polynomial function *at least quadratic* in $\varepsilon_t, \dots, \varepsilon_t^{n-1}$.

We are now ready to define the functionals ℓ_1 and ℓ_2 considered in Lemma 3. Provided that the initial state estimate $\tilde{X}(0)$ is not equal to zero, define

$$\beta_2 = |K| \left(|c_{2,0}| + \left| c_{2,1} \left(\frac{1}{u} \right) \right| \right) |\tilde{X}(0)| + \frac{|\tilde{X}(0)|^2}{2} \quad (77)$$

$$\ell_2(t) = \frac{1}{\beta_2} \left[K \left(c_{2,0} + c_{2,1} \left(\frac{1}{\varepsilon(t-D) + u^r} \right) \right) \tilde{X}(t) + \frac{|\tilde{X}(t)|^2}{2} \right] \quad (78)$$

$$\begin{aligned} \beta_1 \ell_1(\cdot) &= \frac{1}{2} \left| \pi_3 \left(\varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \frac{1}{1+D}, \frac{1}{\varepsilon(t-D) + u^r} \right) \right|^2 \\ &+ (\pi_1 - c_{1,2})(\varepsilon_t, \dots, \varepsilon_t^{(n-1)}) \\ &+ K \left[\pi_2 \left(\varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \tilde{X}, \frac{1}{1+D}, \frac{1}{\varepsilon(t-D) + u^r} \right) - c_{2,0} \right. \\ &\left. - c_{2,1} \left(\frac{1}{\varepsilon(t-D) + u^r} \right) \right] \tilde{X}(t) \end{aligned} \quad (79)$$

Alternatively, if $|\tilde{X}(0)| = 0$, one can define $\beta_2 = 0$ and $\ell_2 = 0$.

We now prove that conditions 1) to 3) of Lemma 3 hold. Indeed, from the error equation of \tilde{X} given in (95), one can actually obtain that

$$\forall t \geq 0, \quad |\tilde{X}(t)| \leq |\tilde{X}(0)| e^{\underline{\lambda}(A+LC)t} \quad (80)$$

if L is chosen such that the eigenvalues of $A + LC$ are distinct and in which $\underline{\lambda}(A + LC) < 0$. From the previous definitions,

using now the fact that $|\frac{1}{\varepsilon(t-D)+u^r}| \leq \frac{1}{\underline{u}}$, one can get that $|\ell_2(t)| \leq e^{\lambda(A+LC)t}$ for $t \geq 0$. Further, one can observe

$$|\beta_1 \ell_1| \leq \frac{1}{2} |\pi_3|^2 + |\pi_1 - c_{1,2}| + |K| |\pi_2 - c_{2,0} - c_{2,1}| |\tilde{X}(0)| \quad (81)$$

in which $|\pi_3|^2$, $|\pi_1 - c_{1,2}|$ and $|\pi_2 - c_{2,0} - c_{2,1}|$ are polynomial functions at least quadratic in $\varepsilon_t, \dots, \varepsilon_t^{(n-1)}$. Now, from the previous observation on $|\frac{1}{\varepsilon(t-D)+u^r}|$, and observing that

$$\frac{1}{1+\tilde{D}} = \frac{\varepsilon(t-D)+u^r}{2\varepsilon(t-D)-\varepsilon(t)+u^r} \quad (82)$$

it is possible to properly define a neighborhood of the origin $\Omega \triangleq (-\omega(K), \omega(K))$ in which $\beta_1 \ell_1$ satisfies the sup-norm

$$\left| \beta_1 \ell_1(\cdot) \right| \leq \beta_{\max}^1 \max |E_t| \quad (83)$$

in which $E \triangleq [\varepsilon \ \dot{\varepsilon} \dots \varepsilon^{(n-1)}]^T$. Note that this neighborhood depends both on the functional ℓ_1 and on the constant β_{\max}^1 and therefore on the feedback gain K . Finally, one obtains that $|\beta_2| < \beta_{\max}^2$ if

$$|\tilde{X}(0)| < \min \{1, \kappa(K) \beta_{\max}^2\} \triangleq \rho^*(K, \omega(K)) \quad (84)$$

$$\kappa(K) \triangleq \frac{1}{|K| \left(|c_{2,0}| + \left| c_{2,1} \left(\frac{1}{\underline{u}} \right) \right| \right) + \frac{1}{2}} \quad (85)$$

in which β_{\max}^2 , and therefore ρ^* , depend on $\omega(K)$. Therefore, for $\max E_0([-D, 0]) < \omega(K)$ and $|\tilde{X}(0)| < \rho^*(K, \omega(K))$, Lemma 3 guarantees the existence of $r(K) > 0, R(K) > 0$ and $\tilde{\gamma} > 0$ such that

$$\forall t \geq 0, \quad |E(t)| \leq \max \{r \max |E_0|, R\beta_2\} e^{-\tilde{\gamma}t} \quad (86)$$

as long as the actuator φ is not saturated and because (72) applies. Consequently, if $\tilde{X}(0)$ satisfies the more restrictive condition

$$|\tilde{X}(0)| < \min \left\{ \rho^*(K, \omega(K)), \kappa(K) \frac{r(K)}{R(K)} \max |E_0| \right\} \quad (87)$$

then, one obtains

$$\forall t \geq 0, \quad |E(t)| \leq r(K) \max |E_0| e^{-\tilde{\gamma}t} \quad (88)$$

as long as the actuator φ is not saturated. Yet, one can observe that a sufficient condition to guarantee that the actuator is not saturated is $|\varepsilon(t)| \leq u^r - \underline{u}, t \geq 0$. Therefore, by choosing

$$\max |E_0| \leq \frac{1}{r(K)} \min \left\{ \frac{u\Delta^*(K)}{2}, u^r - \underline{u}, \omega(K) \right\} \quad (89)$$

one can ensure together that this condition is fulfilled for any $t \geq 0$, that the initial condition lies in the neighborhood Ω and that $|\varepsilon(t)| \leq \frac{u\Delta^*(K)}{2}, t \geq 0$. In particular, the condition (47) is also fulfilled.

Finally, the two choices bearing on $\max |E_0|$ and $|\tilde{X}(0)|$ can be expressed in terms of Θ by defining

$$\begin{aligned} \Theta(K) \triangleq & \frac{1}{r(K)} \min \left\{ \frac{u\Delta^*(K)}{2}, u^r - \underline{u}, \omega(K) \right\} \\ & + \min \left\{ \rho^*(K, \omega(K)), \frac{\kappa(K)}{R(K)} \min \left\{ \frac{u\Delta^*(K)}{2}, u^r - \underline{u}, \omega(K) \right\} \right\} \end{aligned} \quad (90)$$

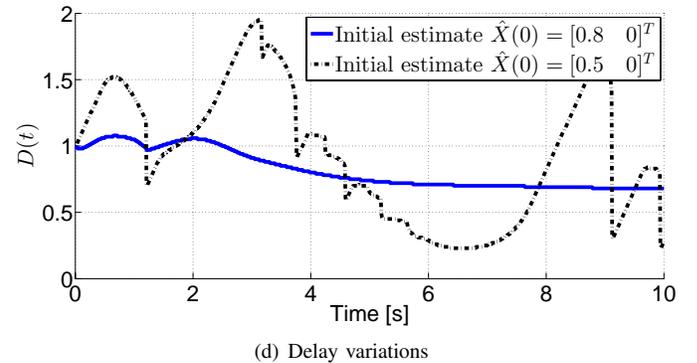
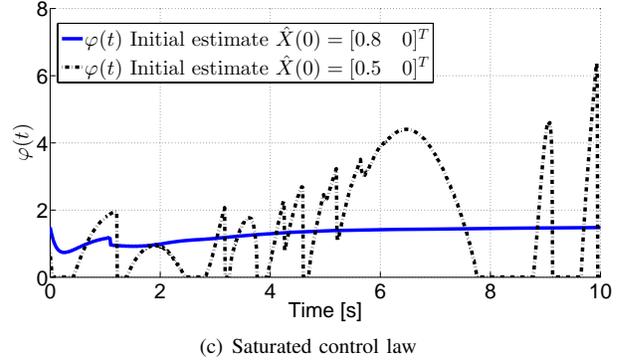
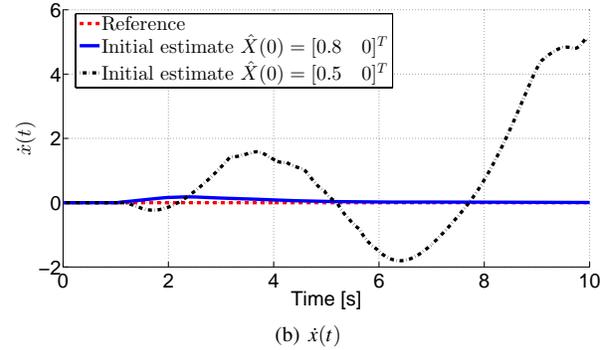
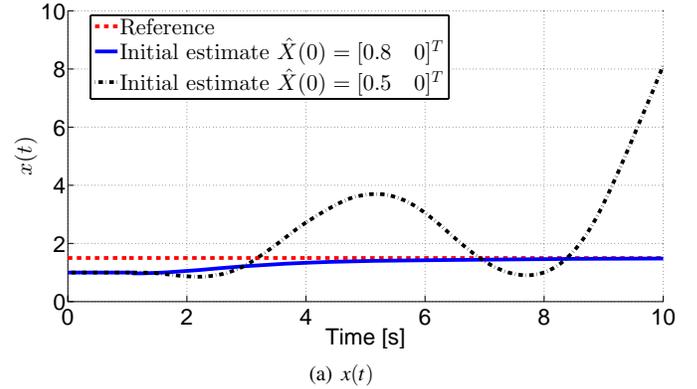


Fig. 3. Simulation results for the same feedback gain ($K = -[1 \ 2]$) and two sets of initial conditions, respectively $\hat{X}(0) = [0.8 \ 0]^T$ and $\hat{X}(0) = [0.5 \ 0]^T$.

This gives the conclusion. \blacksquare

The proof of Theorem 1 directly follows from Lemma 5.

IV. ILLUSTRATIVE EXAMPLE

In this section, for illustration purposes, we consider the following simple unstable second-order plant

$$\begin{cases} \ddot{x} - \dot{x} + x = \varphi(t - D(t)) \\ \int_{t-D(t)}^t \varphi(s) ds = 1, \quad \varphi(t) = \text{Sat}_{(0,01,+\infty)}(u(t)) \end{cases} \quad (91)$$

Following the proposed methodology, we introduce the matrices

$$A = \begin{pmatrix} 0 & 1 \\ -1 & 1 \end{pmatrix}, \quad B = \begin{pmatrix} 0 \\ 1 \end{pmatrix} \quad (92)$$

and implement the control law defined through (40)-(41).

One can note that the chosen initial condition $u_0([-\bar{D}, 0], \mathbb{R})$ is not consistent with the value $u(0)$ imposed by the prediction-based control law, resulting into a discontinuity for $t = 0$. Hence, strictly speaking, the smoothness requirement of the Theorem 1 is not satisfied. However, this does not prevent the conclusion of Theorem 1 to hold, as detailed below. Further, it is worth noting that this condition could still be satisfied by employing an additive input filter.

Simulation results for two different sets of initial conditions, respectively $\hat{X}(0) = [0.8 \ 0]^T$ and $\hat{X}(0) = [0.5 \ 0]^T$ for $X(0) = [1 \ 0]^T$, are pictured in Figure 3. Initial control values are similar in both cases $u(t) = 1, t \in [-\bar{D}, 0]$, resulting into an initial delay $D(0) = 1$ the effects of which can be noticed on the beginning of the state response. The control aims at stabilizing the plant at the target equilibrium $x^* = 1.5$ and (stabilizing) feedback gain has been chosen as $K = -[1 \ 2]$. Observer gain is similar in the two cases $L = -[10 \ 12]$.

Obviously, one can observe that stabilization is achieved for the first set of initial conditions, while, for the second set, the initial estimation error is too important. These results emphasize the local nature of Theorem 1 and can be reasonably related to the delay variations pictured in Figure 3(d)¹⁰. Indeed, the goal of Theorem 1 is to ensure that Condition (9) in Lemma 1, which restricts the delay variations, is satisfied. Here, for the second set of initial conditions, the initial state estimation error implies more important control fluctuations and therefore delay variations which are too important to be handled.

Nevertheless, for this set of initial conditions, it is still possible to change the magnitude of the feedback gain to increase the stabilization region defined through $\theta(K)$ in Theorem 1 so that it contains $\Theta(0)$. This is what is looked for in the simulations reported in Figure 4 in which the initial conditions are similar to the second set previously considered ($\hat{X}(0) = [0.5 \ 0]^T$ with the rest of the setting unchanged) and two different feedback gains are used, respectively $K = -[0.5 \ 1]$ (detuned controller) and $K = -[1 \ 2]$ (both yielding a Hurwitz matrix $A + BK$). Intuitively, pursuing the consideration presented earlier in Section III, the stabilization region could increase while decreasing K . Indeed, this is

¹⁰Alternatively, simulations were performed keeping the same initial state estimate but changing the state reference and lead to the same conclusions.

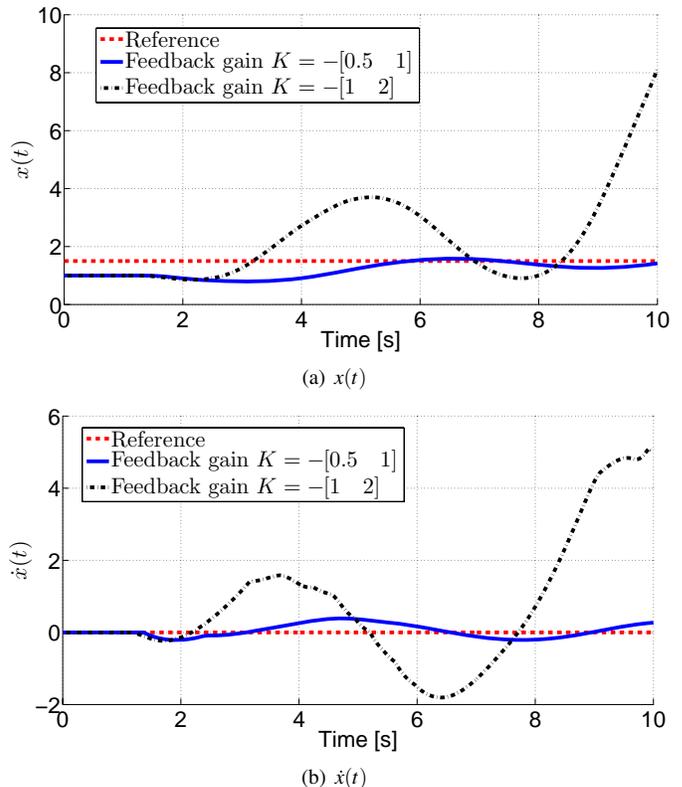


Fig. 4. Simulation results for the same initial conditions ($\hat{X}(0) = [0.5 \ 0]^T$) and two values of the feedback gain respectively $K = -[0.5 \ 1]$ and $K = -[1 \ 2]$.

what is observed in simulation, as stabilization is obtained for $K = -[0.5 \ 1]$ while not for $K = -[1 \ 2]$, as before. Therefore, for given initial condition, restricting the feedback gain magnitude may enable stabilization: the statement of Theorem 1 can be understood as a small-gain result.

Finally, to stress the interest of the proposed method compared to approaches recasting the delay input-variations as a disturbance, we also compare the performance of our controller with a prediction-based controller employing a nominal delay value $D^* = 1/u^*$ as prediction horizon. Simulation results are depicted in Fig. 5. One could reasonably expect that, by employing the current delay in lieu of its asymptotic value, the control law would consequently better compensate the input delay. Indeed, this is what could be observed in Fig. 5: both controllers achieve stabilization but the one proposed in this paper achieves smoother and better performance compared to the (relatively slight) oscillatory behavior of the second one. This gain is modest but one could reasonably hope to improve it by carefully tuning the controller gain.

V. CONCLUSION

In this paper, the problem of robust delay compensation of a linear system driven by a delayed input by means of output feedback has been addressed for a particular class of input-dependent delay defined through an integral relation.

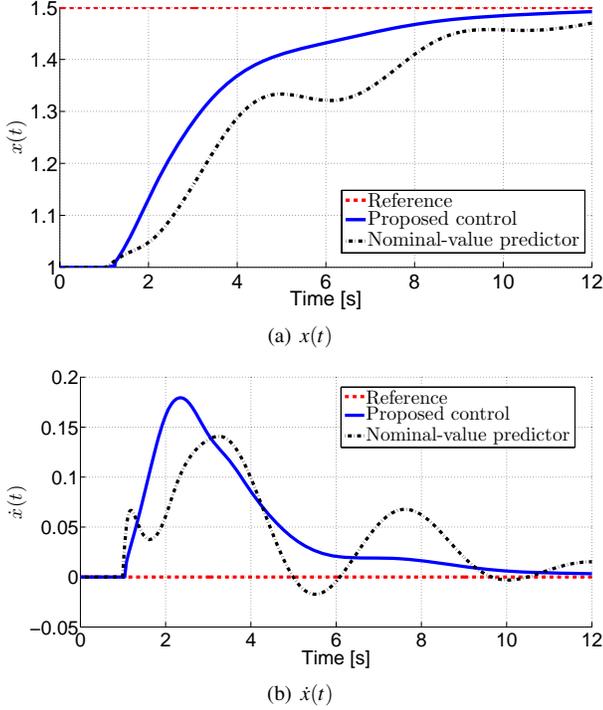


Fig. 5. Simulation results for the proposed prediction-based controller and one employing a nominal delay value $D^r = 1/u^r$ as prediction horizon. The initial conditions are the same ($\hat{X}(0) = [0.5 \ 0]^T$) and the feedback gain is chosen as $K = -[1 \ 2]$.

The proposed approach is based on a two-steps methodology, which, first, requires the delay variations to be bounded and, in turn, relates these variations to input fluctuations. The obtained sufficient conditions yield local asymptotic stability by putting limits on initial conditions depending on the feedback gain.

A natural extension of this work would be to study more complex integral-type delay defining equations, in which the integral kernel depends less directly on the input. A second interesting step would be to investigate the compliance of the considered prediction framework with other input-varying delay models, e.g. models of variable time lag appearing in combustion instability studies [17], [27].

APPENDIX PROOF OF LEMMA 4

Before starting the actual proof, we establish preliminary results. In the following, we note $Z = \hat{X} - X^r$ the estimate state tracking error which satisfies, following (37) and (41),

$$\begin{cases} \dot{Z}(t) = AZ(t) + B\varepsilon(t - D(t)) - LC\tilde{X}(t) \end{cases} \quad (93)$$

$$\begin{cases} \varepsilon(t) = K \left[e^{AD(t)}Z(t) + \int_{t-D(t)}^t e^{A(t-s)}B\varepsilon(s)ds \right] \end{cases} \quad (94)$$

$$\begin{cases} \dot{\tilde{X}}(t) = (A + LC)\tilde{X}(t) \end{cases} \quad (95)$$

when the actuator is not saturated over the whole time interval $[t - D(t), t]$.

A. Preliminary results

Lemma 6: If the actuator is unsaturated over the interval $[t - D(t), t]$ and if $u_0 \in \mathcal{C}^n([-\bar{D}, 0], \mathbb{R})$, the control variable

stated in (41) is n times continuously differentiable and satisfies the following differential equations

$$\begin{aligned} \text{for } 1 \leq m \leq n, \quad \varepsilon^{(m)} - \sum_{l=1}^m KA^{l-1}B\varepsilon^{(m-l)} = \\ f_Z^m(t) + f_\varepsilon^m(t) + f_{\tilde{X}}^m(t) + (1 + \dot{D})^m Ke^{AD}A^m Z \\ + K \int_{t-D}^t A^m e^{A(t-s)}B\varepsilon(s)ds \end{aligned} \quad (96)$$

with

$$\begin{cases} f_Z^1(t) = 0 \quad \text{and for } 2 \leq m \leq n \\ f_Z^m(t) = \frac{d[(1 + \dot{D})^{m-1}]}{dt} Ke^{AD}A^{m-1}Z + \frac{d}{dt}(f_Z^{m-1}(t)) \end{cases} \quad (97)$$

$$\begin{cases} f_\varepsilon^1(t) = \dot{D}Ke^{AD}B\varepsilon(t - D) \quad \text{and for } 2 \leq m \leq n \\ f_\varepsilon^m(t) = \frac{d}{dt}(f_\varepsilon^{m-1}(t)) \\ \quad + [(1 + \dot{D})^{m-1} - (1 - \dot{D})] \varepsilon(t - D)Ke^{AD}A^{m-1}B \\ f_{\tilde{X}}^1(t) = -Ke^{AD}LC\tilde{X}(t) \quad \text{and for } 2 \leq m \leq n \\ f_{\tilde{X}}^m(t) = \frac{d}{dt}(f_{\tilde{X}}^{m-1}(t)) - (1 + \dot{D})^{m-1}Ke^{AD}A^{m-1}LC\tilde{X}(t) \end{cases} \quad (98)$$

$$\begin{cases} f_{\tilde{X}}^m(t) = \frac{d}{dt}(f_{\tilde{X}}^{m-1}(t)) - (1 + \dot{D})^{m-1}Ke^{AD}A^{m-1}LC\tilde{X}(t) \end{cases} \quad (99)$$

Proof The result is constructively obtained by induction and successive substitutions.

Initial step: one directly gets, taking a time-derivative of the control law (94) and using (93),

$$\begin{aligned} \dot{\varepsilon}(t) = KB\varepsilon(t) + (1 + \dot{D})Ke^{AD}AZ + \overbrace{\dot{D}Ke^{AD}B\varepsilon(t - D)}^{=f_\varepsilon^1(t)} \\ + \underbrace{f_Z^1(t)}_{=0} - \underbrace{Ke^{AD}LC\tilde{X}(t)}_{=f_{\tilde{X}}^1(t)} + K \int_{t-D}^t A e^{A(t-s)}B\varepsilon(s)ds \end{aligned} \quad (100)$$

which gives (96) for $m = 1$. Further, as $u_0 \in \mathcal{C}^n([-\bar{D}, 0], \mathbb{R})$, therefore $\varepsilon_0 \in \mathcal{C}^n([-\bar{D}, 0], \mathbb{R})$. Further, ε is continuous for $t \geq 0$ according to the control law (94) and, following the expression of \dot{D} given in (46), \dot{D} is continuous. Therefore, one obtains that ε is continuously differentiable for $t \geq 0$. This implies in particular that \dot{D} is continuously differentiable according to (46) and, therefore, that f_ε^1 also is as $u_0 \in \mathcal{C}^1([-\bar{D}, 0], \mathbb{R})$.

Induction: assume that the property is true for a given $m \geq 1$. We now show that it also holds for $m + 1$. Taking a time-

derivative of (96) for some $m \geq 1$ yields

$$\begin{aligned}
\varepsilon^{(m+1)} - \sum_{l=1}^m KA^{l-1}B\varepsilon^{(m+1-l)} &= \frac{d}{dt}(f_\varepsilon^m(t)) \\
+ \underbrace{\frac{d}{dt}(f_Z^m(t)) + \frac{d(1+\dot{D})^m}{dt}Ke^{AD}A^mZ + KA^mB\varepsilon(t)}_{=f_Z^{m+1}(t)} \\
+ \dot{D}(1+\dot{D})^mKe^{AD}A^{m+1}Z + (1+\dot{D})^mKe^{AD}A^m[AZ \\
+ B\varepsilon(t-D)] - \underbrace{(1+\dot{D})^mKe^{AD}A^mLC\tilde{X}(t) + \frac{d}{dt}(f_{\tilde{X}}^m(t))}_{=f_{\tilde{X}}^{m+1}(t)} \\
- (1-\dot{D})Ke^{AD}A^mB\varepsilon(t-D) + K \int_{t-D}^t A^{m+1}e^{A(t-s)}B\varepsilon(s)ds
\end{aligned} \quad (101)$$

Rearranging terms, one obtains (96) for $m+1$. Similar considerations as those previously used yield that ε is $m+1$ times continuously differentiable. The same holds for D and one can show that f_ε^{m+1} is continuously differentiable. This gives the conclusion. \blacksquare

Further, the sequences (f_ε^m) , (f_Z^m) and $(f_{\tilde{X}}^m)$ satisfy the following properties.

Lemma 7: For $2 \leq m \leq n$, the function f_ε^m introduced in (98) in Lemma 6 is a polynomial function at least quadratic in $\varepsilon_t, \dots, \varepsilon_t^{(m-1)}, \dot{D}, \dots, D^{(m)}$.

Proof The proof is straightforwardly obtained using the definition of (f_ε^m) in Lemma 6 together with the fact that

$$(1+\dot{D})^{m-1} - (1-\dot{D}) = \sum_{l=1}^{m-1} \binom{n}{l} \dot{D}^l + \dot{D} \quad (102)$$

which contains no degree 0 terms. \blacksquare

Lemma 8: For $1 \leq m \leq n$, the function $f_{\tilde{X}}^m$ introduced in (99) in Lemma 6 is in the following form

$$f_{\tilde{X}}^m = K\tilde{\pi}(\dot{D}, \dots, D^{(m-1)})\tilde{X}(t) \quad (103)$$

with $\tilde{\pi}$ a polynomial function with values in $\mathcal{M}_n(\mathbb{R})$

Proof This property directly follows from the definition of $(f_{\tilde{X}}^m)$ and (95). \blacksquare

Lemma 9: Assume that $1+\dot{D} > 0$. For $2 \leq m \leq n$, the function f_Z^m introduced in (97) in Lemma 6 is a polynomial function in $\varepsilon_t, \dots, \varepsilon_t^{(m-1)}, \tilde{X}, \dot{D}, \dots, D^{(m)}$ and $\frac{1}{1+\dot{D}}$, at least quadratic in the variables $\varepsilon_t, \dots, \varepsilon_t^{(m-1)}, \tilde{X}, \dot{D}, \dots, D^{(m)}$.

Proof Again, we reason by induction.

Induction: we assume that the property is true for a given $m \geq 2$. Then, using (96) for m , one obtains

$$\begin{aligned}
f_Z^{m+1}(t) &= \frac{d[(1+\dot{D})^m]}{dt}Ke^{AD}A^mZ + \frac{d}{dt}(f_Z^m(t)) \\
&= \frac{m\dot{D}}{1+\dot{D}} \left[\varepsilon^{(m)} - \sum_{l=1}^m KA^{l-1}\varepsilon^{(m-l)} - f_Z^m(t) - f_\varepsilon^m(t) \right. \\
&\quad \left. - f_{\tilde{X}}^m - K \int_{t-D}^t A^m e^{A(t-s)}B\varepsilon(s)ds \right] + \frac{d}{dt}(f_Z^m(t)) \quad (104)
\end{aligned}$$

Then, using the induction assumption jointly with the two previous lemmas, one can conclude that f_Z^{m+1} is a polynomial function in $\tilde{X}, \varepsilon_t, \dots, \varepsilon_t^{(m)}, \dot{D}, \dots, D^{(m+1)}, \frac{1}{1+\dot{D}}$, at least

quadratic in $\tilde{X}, \varepsilon_t, \dots, \varepsilon_t^{(m)}, \dot{D}, \dots, D^{(m+1)}$.

Initial step: the same arguments as above apply for $m=2$. \blacksquare

B. Design of (72) based on Lemma 6, 7, 9 and 8

As the dynamics matrix that we consider in (6) is of companion type, Cayley-Hamilton theorem gives

$$A^n = - \sum_{m=0}^{n-1} a_m A^m \quad (105)$$

Therefore, for $m=n$ (96) simply gives

$$\begin{aligned}
\varepsilon^{(n)} - \sum_{l=1}^n KA^{l-1}B\varepsilon^{(n-l)} &= f_Z^n(t) + f_\varepsilon^n(t) + f_{\tilde{X}}^n(t) \\
- \sum_{m=0}^{n-1} a_m \left[(1+\dot{D})^n Ke^{AD}A^mZ + K \int_{t-D}^t A^m e^{A(t-s)}B\varepsilon(s)ds \right]
\end{aligned} \quad (106)$$

or again, using now (96) for m ranging from 1 to $n-1$,

$$\begin{aligned}
\varepsilon^{(n)} - \sum_{l=1}^n KA^{l-1}B\varepsilon^{(n-l)} &= f_Z^n(t) + f_\varepsilon^n(t) + f_{\tilde{X}}^n(t) \\
- \sum_{m=1}^{n-1} a_m (1+\dot{D})^{n-m} \left[\varepsilon^{(m)} - \sum_{l=1}^m KA^{l-1}B\varepsilon^{(m-l)} \right. \\
- f_Z^m(t) - f_\varepsilon^m(t) - f_{\tilde{X}}^m(t) - K \int_{t-D}^t A^m e^{A(t-s)}B\varepsilon(s)ds \Big] \\
- \sum_{m=1}^{n-1} a_m K \int_{t-D}^t A^m e^{A(t-s)}B\varepsilon(s)ds \\
- a_0 \left[(1+\dot{D})^n Ke^{AD}Z + K \int_{t-D}^t e^{A(t-s)}B\varepsilon(s)ds \right]
\end{aligned} \quad (107)$$

Besides, using the Leibniz formula,

$$(1+\dot{D})^{n-m} = 1 + \sum_{l=1}^{n-m} \binom{n-m}{l} \dot{D}^l \quad (108)$$

and the expression of (94), one can define

$$\begin{aligned}
\pi_1(\dot{D}, \dots, D^{(n)}, \varepsilon_t, \dots, \varepsilon_t^{(n-1)}) &\triangleq f_Z^n(t) + f_\varepsilon^n(t) + f_{\tilde{X}}^n(t) \\
+ \sum_{m=0}^{n-1} a_m (1+\dot{D})^{n-m} (f_Z^m(t) + f_\varepsilon^m(t) + f_{\tilde{X}}^m(t)) \\
- \sum_{m=1}^{n-1} a_m \left[\sum_{l=1}^{n-m} \binom{n-m}{l} \dot{D}^l \right] \left[\varepsilon^{(m)} - \sum_{l=1}^m KA^{l-1}B\varepsilon^{(m-l)} \right. \\
- K \int_{t-D}^t A^m e^{A(t-s)}B\varepsilon(s)ds \Big] - a_0 \sum_{l=1}^n \binom{n}{l} \dot{D}^l \left[\varepsilon(t) \right. \\
- K \int_{t-D}^t e^{A(t-s)}B\varepsilon(s)ds \Big]
\end{aligned} \quad (109)$$

From there, one can obtain the dynamic (72) by observing that

$$\begin{aligned}
\sum_{l=1}^n KA^{l-1}B\varepsilon^{(n-l)} + \sum_{m=1}^{n-1} \sum_{l=1}^m a_m KA^{l-1}B\varepsilon^{(m-l)} \\
= - \sum_{l=1}^n b_0 k_{n-l} \varepsilon^{(n-l)}
\end{aligned} \quad (110)$$

which is proven in the next section and using Lemma 8 applied to the range n to obtain the existence of a suitable function π_2 . Further, from (109), using Lemma 7 and 9, π_1 is a polynomial

in the variables $\varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \dot{D}, \dots, D^{(n)}, \tilde{X}$ and $\frac{1}{1+\tilde{D}}$, at least quadratic in the variables $\varepsilon_t, \dots, \varepsilon_t^{(n-1)}, \tilde{X}, \dot{D}, \dots, D^{(n)}$.

C. Proof of (110) using companion matrix properties

One can reformulate the term under consideration in (110) as follows

$$\begin{aligned} & \sum_{l=1}^n KA^{l-1}B\varepsilon^{(n-l)} + \sum_{m=1}^{n-1} \sum_{l=1}^m a_m KA^{l-1}B\varepsilon^{(m-l)} \\ &= \sum_{l=1}^n KA^{l-1}B\varepsilon^{(n-l)} + \sum_{p=2}^n \sum_{m=n-1-p}^{n-1} a_m KA^{p-n+m-1}B\varepsilon^{(n-p)} \\ &= KB\varepsilon^{(n-1)} + \sum_{l=2}^n \left[KA^{l-1}B + \sum_{m=n-1-l}^{n-1} a_m KA^{l-n+m-1}B \right] \varepsilon^{(n-l)} \end{aligned} \quad (111)$$

To study the second term in (111), consider m_j^i the j^{th} coefficient of $A^i B$. As A is a companion-type matrix, one gets

$$m_j^i = \begin{cases} 0 & \text{if } j \leq n-i-1 \\ m_{j+1}^{i-1} & \text{if } n-i \leq j \leq n-1 \\ -\sum_{l=n-i+1}^n a_{j-1} m_j^{i-1} & \text{if } j = n \end{cases} \quad (112)$$

and that

$$\text{for } i \in \mathbb{N}, 1 \leq j \leq n \text{ and } 1-j \leq p \leq \max\{i, n-j\} \\ m_j^i = m_{j+p}^{i-p} \quad (113)$$

Then, the coefficient of the $(n-p)^{\text{th}}$ derivative can be rewritten as follows

$$\begin{aligned} & KA^{l-1}B + \sum_{m=n-1-p}^{n-1} a_m KA^{p-n+m-1}B \\ &= KA^{l-1}B + \sum_{i=1}^{l-1} a_{n+i-l} KA^{i-1}B \\ &= -k_{n-l} m_{n-l+1}^{l-1} - \sum_{j=n-l+2}^n k_{j-1} \left[m_j^{l-1} + \sum_{i=n-j+1}^{l-1} a_{n+i-l} m_j^{i-1} \right] \end{aligned} \quad (114)$$

We now prove by induction that, for $l \geq 0$ and for $n-l+2 \leq j \leq n$,

$$m_j^{l-1} = -\sum_{i=n-j+1}^{l-1} a_{n+i-l} m_j^{i-1}.$$

For $l = 2$ and $j = n$, the proposition is indeed true as $m_n^{l-1} = -a_{n-1} b_0$ and $-\sum_{i=n-j+1}^{l-1} a_{n+i-l} m_j^{i-1} = -a_{n-1} m_n^0$. Now, assume that the property is true for a given $l \geq 2$ and for all integer j $n-l+2 \leq j \leq n$. Consider j such that $n-l+2 \leq j \leq n-1$, then

$$\begin{aligned} \sum_{i=n-j+1}^l a_{n+i-l-1} m_j^{i-1} &= \sum_{i=n-j}^{l-1} a_{n+i-l} m_j^i \\ &= \sum_{i=n-j}^{l-1} a_{n+i-l} m_{j+1}^{i-1} \\ &= -m_{j+1}^{l-1} = -m_j^l \end{aligned} \quad (115)$$

using (112) and the induction assumption. This gives the desired result for $n-l+2 \leq j \leq n-1$. For $j = n$, one gets using successively (113) and (112)

$$\begin{aligned} \sum_{i=1}^l a_{n+i-l-1} m_n^{i-1} &= \sum_{i=1}^l a_{n+i-l-1} m_i^{n-1} \\ &= \sum_{i=n+1-l}^n a_{j-1} m_j^{l-1} = -m_n^l \end{aligned} \quad (116)$$

which gives the conclusion. Therefore, for $2 \leq l \leq n$,

$$\begin{aligned} KA^{l-1}B + \sum_{m=n-1-p}^{n-1} a_m KA^{p-n+m-1}B &= -k_{n-l} m_{n-l+1}^{l-1} \\ &= -k_{n-l} m_n^0 = -k_{n-l} b_0 \end{aligned} \quad (117)$$

and $KB = -k_{n-1} b_0$. This concludes the proof of (110).

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